

TOPIC : RIGID BODY DYNAMICS
EXERCISE # 1

SECTION (A)

1. $\frac{d\theta}{dt} = 1.5 + 4t$
 $\omega = 9.5 \text{ rad/s}$
2. $\omega_f = \omega_i + \alpha t$
 $60 = 0 + \alpha(5)$
 $\alpha = 12$
 $\theta = \frac{1}{2} \alpha t^2 = \frac{1}{2} \times 12 \times (5)^2 = 150 \text{ rad}$
3. Linear speed $V = r\omega$
 V depends on radius
4. $\theta = \omega t + \frac{1}{2} \alpha t^2 = 10 \text{ rad}$
5. $\omega_0 = 3000 \text{ rad/min}$
 $\frac{3000}{60} \text{ rad/sec} = (50 \text{ rad/sec})$
 $t = 10 \text{ sec}$
 $\omega_f = 0$
 $\omega_f = \omega_0 + \alpha t$
 $0 = 50 - \alpha (10)$
 $\alpha = 5 \text{ rad/sec}^2$
 $0 = \omega_0 t + \frac{1}{2} \alpha t^2$
 $0 = (50)(10) + \frac{1}{2} (-10)(10)^2$
 $500 - 250 = 250 \text{ rad}$
6. $V = \omega R$
 $V = 10 \times 0.2 = 2 \text{ m/sec.}$
7. Sphere is rotating about a diameter
So, $a = \alpha R$ but, R is zero for particles on the diameter.

SECTION (B)

1. $I = mR^2 = 4 \text{ kgm}^2$
2. M.I of both spheres about common tangent
 $I_0 = 2 \left[\frac{2}{5} mR^2 + mR^2 \right] = \frac{14}{5} mR^2$
 $I_0 = 7 I$
3. $I_x + I_y = I_z$
 z axes is perpendicular to plane of body.
8. $I = \frac{MR^2}{2} + 2 \left[\frac{3}{2} MR^2 \right] = \frac{7}{2} MR^2$

Rigid Body Dynamics

$$11. \quad I = \int dm \quad R^2 = MR^2$$

$$12. \quad I = I_{CM} + Md^2$$

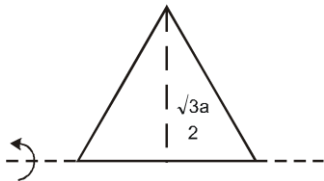
$$I = \frac{ML^2}{12} + M\left(\frac{L}{2}\right)^2$$

$$I = \frac{ML^2}{3}$$

$$13. \quad I = \frac{ML^2}{3} + \frac{ML^2}{3} = \frac{2ML^2}{3}$$

$$14. \quad I = m \left(\frac{\sqrt{3}a}{2} \right)^2$$

$$I = \frac{3ma^2}{4}$$



$$15. \quad I = \frac{ML^2}{12} + M\left(\frac{L}{6}\right)^2 = \frac{ML^2}{9}$$

$$16. \quad \frac{I_1}{I_2} = \frac{m_1 R_1^2}{m_1 R_2^2} = \frac{m_1}{m_2} \times \frac{4}{1} = \frac{2}{1}$$

$$\frac{m_1}{m_2} = \frac{1}{2}$$

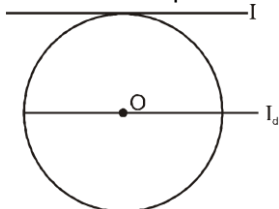
$$17. \quad I = 4 \left[\frac{ML^2}{12} + M\left(\frac{L}{2}\right)^2 \right] = \frac{4}{3} ML^2$$

$$18. \quad I = \frac{2}{5} M \left(\frac{R}{2} \right)^2 + \left[\frac{2}{5} M \left(\frac{R}{2} \right)^2 + M(2R)^2 \right]$$

$$I = \frac{21}{5} MR^2$$

$$19. \quad \text{Moment of inertia of a disc about its diameter is } I_d = \frac{1}{4} MR^2$$

Now, according to perpendicular axis theorem moment of inertia of disc about a tangent passing through rim and in the plane of disc is



Rigid Body Dynamics

$$I = I_d + MR^2 = \frac{1}{4}MR^2 + MR^2 = \frac{5}{4}MR^2$$

$$20. \quad I = \frac{5}{4}MR^2$$

$$I' = \frac{3}{2}MR^2 = \frac{6}{5}I$$

$$21. \quad I = \frac{7}{5}MR^2 \Rightarrow MK^2 = \frac{7}{5}MR^2 \Rightarrow K = \sqrt{\frac{7}{5}}R$$

$$22. \quad I = 4 \times m \left(\frac{L}{\sqrt{2}} \right)^2 = 2mL^2$$

$$mK^2 = 2mL^2$$

$$K = \sqrt{2}L$$

$$23. \quad \frac{I_{\text{ring}}}{I_{\text{Disc}}} = \frac{MR^2}{\frac{MR^2}{2}} = 2$$

$$24. \quad I = \frac{MR^2}{2}$$

$$K = \frac{R}{\sqrt{2}} = 3.54 \text{ cm}$$

25. Moment of inertia of solid sphere about an axis passing through its centre of gravity.

$$I = \frac{2}{5}mr^2 \text{ Where } m = \text{mass of sphere } R = \text{radius of sphere}$$

From theorem of parallel axis, moment of inertia about its tangential axis

$$I = I' + mR^2 = \frac{2}{5}MR^2 + MR^2 = \frac{7}{5}MR^2$$

26. The moment of inertia in rotational motion is equivalent to mass as in linear motion.

$$27. \quad \text{For disc, } I = \frac{1}{2}ma^2 \quad \text{For ring, } I = ma^2$$

$$\text{For square of side } 2a = \frac{M}{12} [(2a)^2 + (2a)^2] = \frac{2}{3}Ma^2$$

For square of rod of length $2a$

$$I = 4 \left[\frac{M(2a)^2}{12} + Ma^2 \right] = \frac{16}{3}Ma^2 \text{ Hence, moment of inertia is maximum for square of four rods.}$$

28. The moment of inertia of the given system that contains 5 particles each of mass 2 kg on the rim of circular disc of radius 0.1 m and of negligible mass is given by = MI of disc + MI of particles
Since, the mass of the disc is negligible therefore, MI of the system = MI of particles
 $= 5 \times 2 \times (0.1)^2 = 0.1 \text{ kg m}^2$

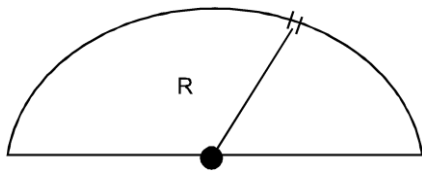
29. Moment of inertia of disc about a tangent and parallel to its plane,

$$I = \frac{MR^2}{4} + MR^2 \quad \dots(i)$$

$$\text{Moment of inertia of disc about a tangent and perpendicular to its plane} = \frac{MR^2}{2} + MR^2 = \frac{3}{2}MR^2$$

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$$\frac{I}{I_{\text{perpendicular}}} = \frac{\frac{5}{4}MR^2}{\frac{3}{2}MR^2} = \frac{5}{6} \quad \therefore I_{\text{perpendicular}} = \frac{6}{5}I$$



30.

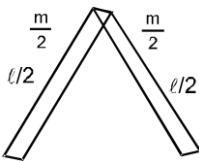
$$I = \int dm R^2$$

$$I = R^2 \int dm = R^2 M = MR^2$$

31.

$$I_B = I_A + Md^2$$

$$\text{Then } I_B > I_A$$



32.

$$I_0 = I_1 + I_2 \Rightarrow I_0 = \frac{(m/2)\left(\frac{l}{2}\right)^2}{3} + \frac{(m/2)\left(\frac{l}{2}\right)^2}{3} = \frac{(m/l^2)}{12}$$

33.

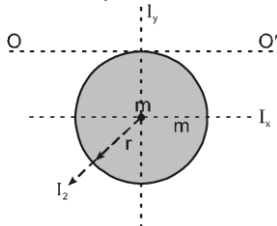
$$I_x + I_y = I_z$$

$$2I_x = I_z \quad \therefore I_1 = 2 \times 200 = 400 \text{ gm cm}^2.$$

34.

Perpendicular axis theorem

$$I_2 = I_x + I_y = \frac{mr^2}{2}$$

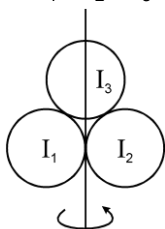


$$\text{from symmetry } I_x = I_y \Rightarrow I_x = \frac{mr^2}{4} \quad \text{Parallel axis theorem}$$

$$I_{O'O'} = I_x + mr^2 = \frac{mr^2}{4} + mr^2 = \frac{5}{4} mr^2$$

35.

$$I = I_1 + I_2 + I_3 \Rightarrow I_1 = I_2 = \frac{3}{2} mr^2 \Rightarrow I_3 = \frac{mr^2}{2}$$



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$$\therefore I = I_1 + I_2 + I_3 = \frac{7}{2} mr^2$$

Moment of inertia = $3mk^2$ where k is radius of gyration.

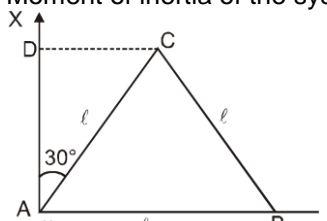
$$3mk^2 = \frac{7}{2} mr^2 \Rightarrow k = \sqrt{\frac{7}{6}} r$$

Rigid Body Dynamics

37. Moment of inertia depends on distribution of mass about axis of rotation. Density of iron is more than that of aluminium, therefore for moment of inertia to be maximum, the iron should be far away from the axis. Thus, aluminium should be interior and iron surrounds it.
38. By perpendicular axis theorem moment of inertia about any axis passing through centre and in the plane of plate will be I (by symmetry)

39. We know that M.I. of a circular wire of mass M and radius R about its diameter is $\frac{MR^2}{2}$
40. If a body has mass M and radius of gyration is K , then $I = MK^2$
 Moment of inertia of a disc and circular ring about a tangential axis in their planes are respectively.
- $$I_d = \frac{5}{4}M_d R^2 \Rightarrow I_r = \frac{3}{2}M_r R^2 \quad \text{but } I = MK^2 \Rightarrow K = \sqrt{\frac{I}{M}}$$
- $$\therefore \frac{K_d}{K_r} = \sqrt{\frac{I_d}{I_r} \times \frac{M_r}{M_d}} \quad \text{or} \quad \frac{I_d}{I_r} = \sqrt{\frac{(5/4)M_d R^2}{(3/2)M_r R^2} \times \frac{M_r}{M_d}} = \sqrt{\frac{5}{6}} \quad \therefore I_d : I_r = \sqrt{5} : \sqrt{6}$$

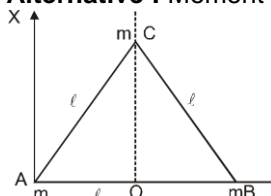
41. Moment of inertia of the system about AX is given by



$$MI = mAr^2_A + mBr^2_B + mCr^2_C$$

$$MI = m(0)^2 + m(\ell)^2 + m(\ell \sin 30^\circ)^2 = m\ell^2 + \frac{m\ell^2}{4} = \frac{5}{4}m\ell^2$$

Alternative : Moment of inertia of a system about a line OC perpendicular to AB, in the plane of ABC is



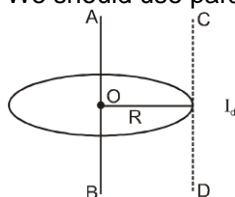
$$I_{CO} = m \times 0 + m \times \left(\frac{\ell}{2}\right)^2 + m \times \left(\frac{\ell}{2}\right)^2 \quad \therefore I_{CO} = \frac{m\ell^2}{4} + \frac{m\ell^2}{4} = \frac{m\ell^2}{2}$$

According to parallel-axis theorem

$I_{AX} = I_{CO} + Mx^2$ where x = distance of AX from CO, M = total mass of system

$$I_{AX} = \frac{m\ell^2}{2} + 3m \times \left(\frac{\ell}{2}\right)^2 \Rightarrow I_{AX} = \frac{m\ell^2}{2} + \frac{3m\ell^2}{4} = \frac{5}{4}m\ell^2$$

42. We should use parallel axis theorem



Moment of inertia of disc passing through its centre of gravity and perpendicular to its plane is

$$I_{AB} = \frac{1}{2}MR^2 \quad \text{Using theorem of parallel axes, we have,}$$

$$I_{CD} = I_{AB} + MR^2 = \frac{1}{2}MR^2 + MR^2 = \frac{3}{2}MR^2$$

Rigid Body Dynamics

Note : The role of moment of inertia in the study of rotational motion is analogous to that of mass in study of linear motion.

45. Let same mass and same outer radii of solid sphere and hollow sphere are M and R respectively. The moment the moment of inertia of hollow sphere (spherical shell) B about its diameter

$$I_A = \frac{2}{5} MR^2 \quad \dots\dots\dots(i)$$

Similarly the moment of inertia of hollow sphere (spherical shell) B about its diameter

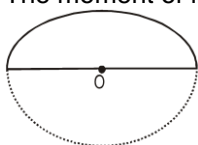
$$I_B = \frac{2}{5} MR^2 \quad \dots\dots\dots(ii)$$

It is clear from eqs. (i) and (ii), $I_A < I_B$

46. The mass of complete (circular) disc is

$$M + M = 2M$$

$$\text{The moment of inertia of disc is } I = \frac{2Mr^2}{2}$$



$$= Mr^2$$

Let the moment of inertia of semicircular disc is I_1 .

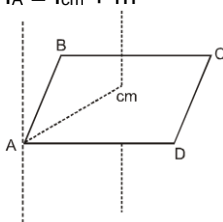
The disc may be assumed as combination of two semicircular parts.

$$\text{Thus, } I_1 = I - I_1 \quad \therefore \quad I_1 = \frac{I}{2} = \frac{Mr^2}{2}$$

47. $I = 2m \left(\ell / \sqrt{2} \right)^2 + m \left(\sqrt{2} \ell \right)^2 = 3m\ell^2$.

$$48. \quad I_{AC} = \frac{1}{2} \left(\frac{M\ell^2}{6} \right) = \frac{M\ell^2}{12}, \quad I_{EF} = \frac{M\ell^2}{12}, \quad I_{AC} = I_{EF}.$$

$$49. \quad I_A = I_{cm} + m \left(\frac{a}{\sqrt{2}} \right)^2$$



$$= \frac{ma^2}{6} + \frac{ma^2}{2} = \frac{2}{3} ma^2$$

SECTION (C)

$$2. \quad \left(\frac{1}{2} MR^2 \right) \alpha = \tau$$

$$\alpha = 0.25 \text{ rad/s}^2$$

$$4. \quad \tau = I \alpha$$

$$I = \frac{31.4}{4\pi} = 2.5 \text{ kgm}^2$$

$$5. \quad \ell = 3 \text{ kg m}^2, \tau = 6 \text{ Nm}, t = 20 \text{ sec.} \quad \text{From } \tau = I \alpha$$

$$\alpha = \frac{\tau}{I} = \frac{6}{3} = 2 \text{ rad/sec}^2 \quad \therefore \text{Angular displacement}$$

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$$= \omega_0 t + \frac{1}{2} \alpha t^2 = 0 \times 20 + \frac{1}{2} (2)(20)^2 = 400 \text{ radian}$$

$$6. \quad \vec{F} = 4\hat{i} - 10\hat{j} \Rightarrow \vec{r} = (-5\hat{i} - 3\hat{j}) \Rightarrow \tau = \vec{r} \times \vec{F} = (-5\hat{i} - 3\hat{j}) \times (4\hat{i} - 10\hat{j}) = 50\hat{k} + 12\hat{k} = 62\hat{k}$$

$$7. \quad \vec{F} = 2\hat{i} + 3\hat{j} - \hat{k} \text{ at point } (2, -3, 1) \text{ torque about point } (0, 0, 2)$$

$$\vec{r} = (2\hat{i} - 3\hat{j} + \hat{k}) - 2\hat{k} \Rightarrow \tau = \vec{r} \times \vec{F} = (2\hat{i} - 3\hat{j} - \hat{k}) \times (2\hat{i} + 3\hat{j} - \hat{k})$$

$$\vec{\tau} = (6\hat{i} + 12\hat{k}) \Rightarrow \left| \vec{\tau} \right| = (6\sqrt{5})$$

8. Torque of a couple always remains constant about any point

$$9. \quad \tau = I\alpha$$

$$30 = 2 \times \alpha \Rightarrow \alpha = 15 \text{ rad/sec}^2$$

From equation of angular motion

$$\theta = \omega_0 t + \frac{1}{2} \alpha t^2 = 0 + \frac{1}{2} \times 15 \times 10 \times 10 = 750 \text{ rad}$$

$$10. \quad \vec{\tau} = \vec{r} \times \vec{F} \text{ implies that } \vec{r}, \vec{F} \text{ and } \vec{\tau} \text{ all are mutually perpendicular to each other. } \therefore \vec{\tau} \cdot \vec{r} = 0, \vec{F} \cdot \vec{\tau} = 0$$

SECTION (D)

$$1. \quad \text{Torque about O}$$

$$F \times 40 + F \times 80 - (F \times 20 + F \times 60)$$

In clockwise direction = $F \times 40$

$$2. \quad \vec{F}_1 = 2\hat{i} + 3\hat{j} + 4\hat{k}$$

$$\vec{F}_2 = -2\hat{i} - 3\hat{j} - 4\hat{k}$$

$$\vec{r}_1 = 3\hat{i} + 3\hat{j} + 4\hat{k} \quad \vec{r}_2 = \hat{i}$$

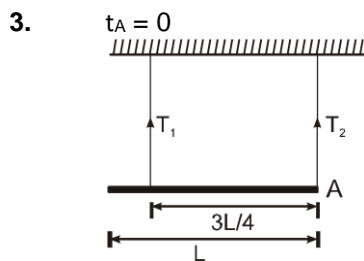
$$\vec{\tau}_1 = \vec{r}_1 \times \vec{F}_1 = (3\hat{i} + 3\hat{j} + 4\hat{k}) \times (2\hat{i} + 3\hat{j} + 4\hat{k})$$

$$\vec{\tau}_1 = 9\hat{k} - 12\hat{j} - 6\hat{j} + 12\hat{i} + 8\hat{j} - 12\hat{i}$$

$$\vec{\tau}_1 = -4\hat{j} + 3\hat{k}$$

$$\vec{\tau}_2 = \vec{r}_2 \times \vec{F}_2 = (\hat{i}) \times (-2\hat{i} - 3\hat{j} - 4\hat{k}) = -3\hat{k} + 4\hat{j}$$

$$\left(\vec{\tau}_1 + \vec{\tau}_2 = -4\hat{i} + 3\hat{k} - 3\hat{k} + 4\hat{j} = 0 \right) \text{ body in rotation equilibrium}$$



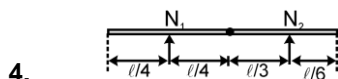
$$T_1 \times \frac{3L}{4} - mg \times \frac{L}{2} = 0 \quad \dots(1)$$

$$T_1 = \frac{2mg}{3}$$

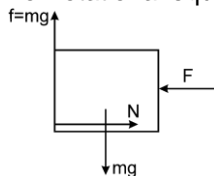
$$T_1 + T_2 = mg \quad \dots(2)$$

Rigid Body Dynamics

$$T_2 = \frac{mg}{3} \Rightarrow \frac{T_1}{T_2} = \frac{2}{1} \text{ Ans.}$$



For rotational equilibrium $N_1 \times \frac{l}{4} = N_2 \times \frac{l}{6} \Rightarrow N_1 : N_2 = 4 : 3$



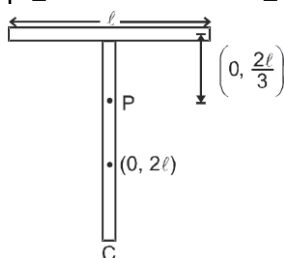
From equilibrium,
friction = mg $N = F$
about centre of mass

$$\tau = 0 \Rightarrow mg \cdot a = \text{torque due to normal}$$

\therefore Normal will produce torque since F passes through centre its torque is zero.

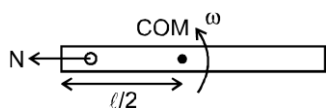
6. For pure translatory motion, net torque about centre of mass should be zero. Thus \vec{F} is applied at centre of mass of system.

$$P = \frac{0 \times l + l \cdot 2l}{l + 2l} = \frac{2l^2}{3l} = \frac{2l}{3}$$



$$\therefore PC = \left(l - \frac{2l}{3} + l \right) = \frac{4l}{3}$$

SECTION (E)



$$N = \left(m\omega^2 \frac{l}{2} \right)$$

2. Initial velocity of each point on the rod is zero so angular velocity of rod is zero.
Torque about O

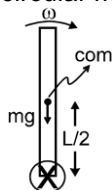
$$T = I \alpha$$

$$20g(0.8) = \frac{ml^2}{3} \alpha \Rightarrow 20g(0.8) = \frac{20(1.6)^2}{3} \alpha$$



$$\Rightarrow \frac{3g}{3.2} = \alpha = \text{angular acceleration}$$

3. For the circular motion of com :

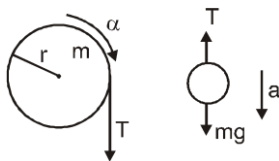


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$$mg = m \left(\frac{L}{2} \right) \omega^2 \Rightarrow \omega = \sqrt{\frac{2g}{L}}$$

Note : Since the reaction at the end is zero, the gravitational force will have to provide the required centripetal force.

5. Beam is not at rotational equilibrium, so force exerted by the rod (beam) decrease



6. There is no slipping between pulley and thread.

$$\text{So, } (a = \alpha r) \quad \dots\dots\dots(i)$$

For point mass :

$$mg - T = ma \quad \dots\dots\dots(ii)$$

Equation of torque for disc

$$Tr = I \cdot \alpha$$

$$Tr = \frac{mr^2}{2} \cdot \alpha$$

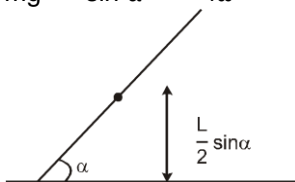
$$T = \frac{mr\alpha}{2} = \left(\frac{mg}{2} \right) \quad \dots\dots\dots(iii)$$

$$mg - \frac{mg}{2} = ma \quad \Rightarrow \quad mg = \frac{3mg}{2} \quad \Rightarrow \quad a = \frac{2g}{3}$$

SECTION (F)

$$\begin{aligned} 2. \quad KE &= \frac{1}{2} I \omega^2 \\ 1500 &= (1.2) \omega^2 \\ \omega &= \sqrt{\frac{3000}{1.2}} \\ \omega_f - \omega_i &= \alpha t \\ \sqrt{\frac{3000}{1.2}} &= 25 t \\ t &= 2 \text{ s} \end{aligned}$$

$$3. \quad mg \frac{L}{2} \sin \alpha = \frac{1}{2} I \omega^2 \quad \Rightarrow \quad mg \frac{L}{2} \sin \alpha = \frac{1}{2} \frac{ML^2}{3} \omega^2$$



$$\omega = \sqrt{\frac{3g \sin \alpha}{L}}$$

$$4. \quad mgh = \frac{1}{2} mV^2 + \frac{1}{2} I \omega^2 \Rightarrow mgh = \frac{1}{2} mr^2 \omega^2 + \frac{1}{2} I \omega^2 \Rightarrow \omega = \sqrt{\frac{2mgh}{I + mr^2}}$$

$$6. \quad \text{Given } a_A = 2\alpha = 5 \text{ m/s}^2 \quad \Rightarrow \quad \alpha = 5/2 \text{ rad/s}^2 \quad \Rightarrow \quad a_B = 1 \cdot (\alpha) = 5/2 \text{ m/s}^2$$

7. Immediately after string connected to end B is cut, the rod has tendency to rotate about point A.

Rigid Body Dynamics

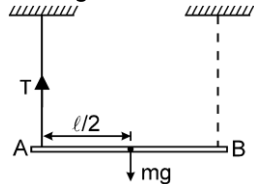
Torque on rod AB about axis passing through A and normal to plane of paper is

$$\frac{m\ell^2}{3} \alpha = mg \frac{\ell}{2} \Rightarrow \alpha = \frac{3g}{2\ell}$$

Aliter : Applying Newton's law on center of mass

$$mg - T = ma \quad \dots(i)$$

Writing $\tau = I\alpha$ about center of mass



$$T \frac{\ell}{2} = \frac{m\ell^2}{12} \alpha \quad \dots(ii)$$

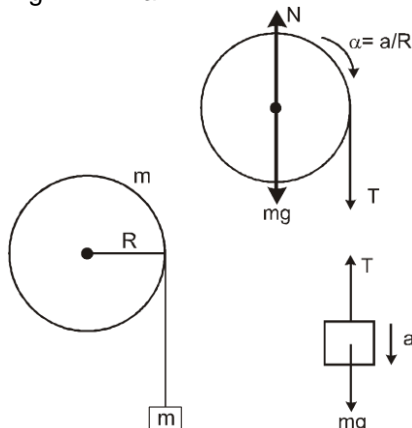
$$\text{Also } a = \frac{\ell}{2} \alpha \quad \dots(iii) \quad \text{From (i), (ii) and (iii) } \alpha = \frac{3g}{2\ell}$$

8. Given : $I = 2 \text{ kg} \cdot \text{m}^2$, $\omega_0 = \frac{60}{60} \times 2\pi \text{ rad/s}$,
 $\omega = 0$, $t = 60 \text{ s}$

The torque required to stop the wheel's rotation is

$$\tau = I\alpha = I \left(\frac{\omega_0 - \omega}{t} \right) \Rightarrow \tau = \frac{2 \times 2\pi \times 60}{60 \times 60} = \frac{\pi}{15} \text{ N-m}$$

10. $mg - T = ma$



$$TR = \frac{mR^2 \alpha}{2} \Rightarrow T = \frac{mR\alpha}{2} = \frac{ma}{2} \Rightarrow mg - \frac{ma}{2} = ma \Rightarrow \frac{3ma}{2} = mg \Rightarrow a = \frac{2g}{3} \quad \text{Ans.}$$

11. Since the work done is independent of the information about which point the rod is rotating, by work-energy theorem the kinetic energy will also be independent of the same. Hence (2)
12. From conservation of angular momentum ($I\omega = \text{constant}$), angular velocity will remain half.

As, $K = \frac{1}{2} I\omega^2$ the rotational kinetic energy will become half. Hence, the correct option is (2).

SECTION (G)

$$\frac{E_A}{E_B} = \frac{\frac{1}{2} I_A \omega_A^2}{\frac{1}{2} I_B \omega_B^2} = \frac{L_A^2}{I_A} \frac{I_B}{L_B^2}$$

$$3. \Rightarrow \frac{L_A}{L_B} = 5$$

4. $I_A \omega_A = I_B \omega_B$
 $I_A > I_B$ therefore $\omega_A < \omega_B$

Rigid Body Dynamics

$$\frac{K_B}{K_A} = \frac{\frac{1}{2} I_B \omega_B^2}{\frac{1}{2} I_A \omega_A^2} = \frac{\omega_B}{\omega_A} < 1$$

7. $\tau = \frac{\Delta L}{\Delta t} = \frac{2}{5} = 0.4 \text{ N-m}$

8. Direction of Angular momentum is along the direction of angular velocity, which is an axial vector.

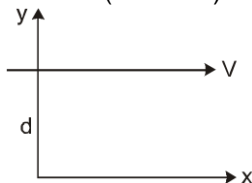
13. $MR^2\omega = (MR^2 + 2mR^2)\omega'$

$$\omega' = \frac{\omega M}{M + 2m}$$

15. $I\omega = \text{constant}$

16. External torque = 0
 $L = \text{constant.}$

19. $L = mVd$ (constant)



21. $KE = \frac{1}{2} I\omega^2 \Rightarrow 360 = \frac{1}{2} I (30)^2$
 $I = 0.8 \text{ kg m}^2$

22. $L = I\omega$
 $L = (mr^2) \omega$

$$F_c = mr\omega^2 = \frac{L^2}{mr^3}$$

23. $\vec{L} = \vec{r} \times \vec{P}$

24. The angular momentum of a particle of mass m moving with velocity u about origin is
 $J = mu \times d = m u d = \text{constant}$

25. From law of conservation of angular momentum, if no external torque is acting upon a body rotating about an axis, then the angular momentum of the body remains constant that is

$$J = I\omega$$

Also, $I = \frac{2}{5} MR^2$ for a solid sphere.

Given, $R_1 = R$ $R_2 = \frac{R}{n} \therefore \frac{2}{5} MR^2\omega_1 = \frac{2}{5} M\left(\frac{R}{n}\right)^2 \times \omega_2 \Rightarrow \omega_2 = n^2\omega_1 = m^2\omega$

26. Angular momentum

$$L = I\omega$$

Kinetic energy

$$K = \frac{1}{2} I\omega^2 = \frac{1}{2} L\omega \quad \{\text{from Eq. (i)}\} \therefore L = \frac{2K}{\omega}$$

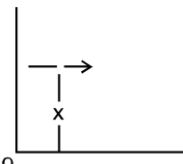
$$\text{Now } L' = \frac{2\left(\frac{K}{2}\right)}{2\omega} \Rightarrow L' = \frac{L}{4}$$

Rigid Body Dynamics

27. $KE_R = \frac{1}{2} I \omega^2$
 $L = I \omega$

$$KE_R = \frac{L^2}{2I}$$

28. $\vec{\tau} = \frac{dL}{dt} = \frac{4A_0 - A_0}{4} = \left(\frac{3A_0}{4} \right)$



29. $\Rightarrow L = (mvx) = \text{cont: because } v = \text{cont and } x = \text{cont.}$

30. $L = I \omega \Rightarrow \omega' = 2\omega$
 $\frac{1}{2} \left(\frac{1}{2} I \omega^2 \right) = \frac{1}{2} I' \omega'^2 \Rightarrow \frac{I \omega^2}{2} = I' 4 \omega^2$
 $I' = \left(\frac{I}{8} \right) \Rightarrow L' = I' \omega' = \frac{I}{8} 2\omega = \frac{I \omega}{4} = \left(\frac{L}{4} \right)$

31. External torque $\vec{\tau}_{\text{ext}} = 0$
 $I_1 \omega_1 = I_2 \omega_2$ when he folds his arms I reduces. So, $I_1 > I_2$ then $(\omega_1 < \omega_2)$. So, $(L = \text{constant})$

32. The direction of L is perpendicular to the line joining the bob to point C. Since this line keeps changing its orientation in space, direction of L keeps changing however as ω is constant, magnitude of L remain constant.

Aliter : The torque about point is perpendicular to the angular momentum vector about point C. Hence it can only change the direction of L , and not its magnitude.

33. The angular momentum about axis CO is the component of angular momentum about point C along the line CO. This is constant both in direction and magnitude.

Aliter : Torque about axis CO is zero hence L about CO is constant in both direction and magnitude.

35. In uniform circular motion the only force acting on the particle is centripetal (towards center). Torque of this force about the center is zero. Hence angular momentum about center remain conserved.

37. Conservation of angular momentum about C.O.M. of m of loop of mass m gives

$$\frac{mVR}{2} = \left[\left\{ m R^2 + m \left(\frac{R}{2} \right)^2 \right\} + m \left(\frac{R}{2} \right)^2 \right] \omega \Rightarrow V = 3 \omega R \Rightarrow \omega = \frac{V}{3R} \text{ Ans. (B)}$$

SECTION (H)

1. $KE_r = \frac{1}{2} I \omega^2 = \frac{1}{2} \left(\frac{2}{5} MR^2 \right) \left(\frac{V}{R} \right)^2 = \frac{1}{5} mV^2 \Rightarrow KE_{\text{Total}} = \frac{1}{2} mV^2 + \frac{1}{5} I \omega^2 = \frac{7}{5} mV^2 \Rightarrow \text{Ratio} = \frac{2}{7}$

3. $KE = \frac{1}{2} mV^2 + \frac{1}{2} I \omega^2 = \frac{1}{2} mV^2 + \frac{1}{2} mR^2 \left(\frac{V}{R} \right)^2 \Rightarrow KE = mV^2 = 4 \text{ Joule}$

4. $KE_t = \frac{1}{2} mV^2 \Rightarrow KE_r = \frac{1}{2} I \omega^2 = \frac{1}{2}$
 $\Rightarrow \left(\frac{1}{2} mR^2 \right) \left(\frac{V}{R} \right)^2 = \frac{1}{4} mV^2 \quad \frac{KE_{\text{rotation}}}{KE_{\text{Total}}} = \frac{1/4 mV^2}{3/4 mV^2} = \frac{1}{3}$

Rigid Body Dynamics

$$6. \quad mgh = \frac{1}{2} mV^2 + \frac{1}{2} I\omega^2 \Rightarrow mgh = \frac{1}{2} mV^2 + \frac{1}{2} \frac{mR^2}{2} \left(\frac{V}{R}\right)^2$$

$$\Rightarrow mgh = \frac{1}{2} mV^2 + \frac{1}{4} mV^2 \Rightarrow V = \sqrt{\frac{4}{3}gh}$$

7. The total energy of a body rolling without slipping

$$K_{\text{total}} = K_{\text{rot}} + K_{\text{trans}} = \frac{1}{2} I \omega^2 + \frac{1}{2} M u^2 \text{ but } I_{\text{disc}} = \frac{1}{2} M R^2 \text{ and } u = r \omega$$

$$\therefore K_{\text{total}} = \frac{1}{2} \left(\frac{1}{2} M R^2 \right) \omega^2 + \frac{1}{2} M (r \omega)^2 = \frac{1}{4} M R^2 \omega^2 + \frac{1}{2} M R^2 \omega^2 = \frac{3}{4} M R^2 \omega^2 = \frac{3}{4} M u^2$$

8. The velocity of solid sphere on the bottom of inclined plane is

$$u = \sqrt{\frac{2gh}{1 + I/MR^2}} \text{ where, } I = M.I \text{ of sphere,}$$

$M = \text{mass of sphere and } R = \text{radius of sphere}$
The moment of inertia so solid sphere about its diameter

$$I = \frac{2}{5} M R^2 \therefore u = \sqrt{\frac{2gh}{1 + \frac{2}{5}}} = \sqrt{\left(\frac{10}{7}gh\right)} \therefore h = \frac{7u^2}{10g}$$

9. The kinetic energy of sphere while rolling on an inclined plane is given by

$$E_g = \text{Translational kinetic energy} + \text{Rotational kinetic energy} = \frac{1}{2} m v^2 + \frac{1}{2} I \omega^2$$

$$E_k = \frac{1}{2} \times 2 \times (0.5)^2 + \frac{1}{2} \times \frac{2}{3} \times 2 \times (0.1)^2 \times \left(\frac{0.5}{0.1}\right)^2 = 0.25 + 0.17 = 0.42 \text{ J}$$

10. In pure rolling, mechanical energy remains conserved. Therefore, when heights of inclines are equal, speed of sphere will be same in both the cases. But as acceleration down the plane, $a \propto \sin \theta$ therefore, acceleration and time of descent will be different.

11. Friction force is zero and impulas is passes through centre so external torque is zero and angular momentum and linear momentum remains const. so
 $\Rightarrow (\omega_A = \omega)$ but due to collision linear velocity inter change.

12. For a body rolling without slipping, the velocity of any point P on the body is $\vec{v}_p = \vec{v}_{cm} + \vec{v}_{p,cm}$ where $\vec{v}_{p,cm} = R\omega$ in direction perpendicular to line joining centre and point P.

Velocity of point A is ,

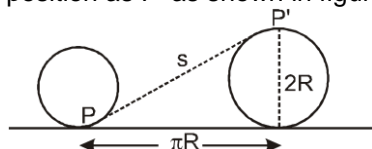
$$V_A = v_{cm} + R\omega = v_{cm} + v_{cm} \therefore (v_{cm} = R\omega) = 2v_{cm}$$

velocity of point B is,

$$V_B = v_{cm} - R\omega = v_{cm} - v_{cm} = 0$$

Thus, the velocity of point a is $2v_{cm}$ and velocity of point B is zero.

13. When the wheel rolls on the ground without slipping and completes half rotation, point P takes new position as P' as shown in figure. Horizontal displacement, $x = \pi R$



Vertical displacement, $y = 2R$

Thus, displacement of the point P when wheel completes half rotation,

$$s = \sqrt{x^2 + y^2} = \sqrt{(\pi R^2) + (2R)^2} = \sqrt{\pi^2 R^2 + 4R^2} \text{ but } R = 1\text{m (given)} \therefore s = \sqrt{\pi^2(1)^2 + 4(1)^2} = \sqrt{\pi^2 + 4} \text{ m}$$

14. Linear kinetic energy

$$K_t = \frac{1}{2}mv^2 = \frac{1}{2}mr^2\omega^2 = \frac{1}{2}I\omega^2$$

$$\text{Rotational kinetic energy } K_r = \frac{1}{2}I\omega^2$$

$$\text{Total kinetic energy } K = K_t + K_r = \frac{1}{2}I\omega^2 + \frac{1}{2}I\omega^2 = I\omega^2$$

$$\frac{K_r}{K} = \frac{1}{2}$$

Rigid Body Dynamics

16. Moment of inertia of sphere

$$I = \frac{2}{5} MR^2 \quad \dots (1)$$

and for pure rolling $v = R \omega \quad \dots (2)$

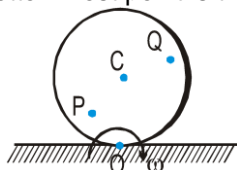
$$\frac{\text{Rotational KE}}{\text{Translational KE}} = \frac{\frac{1}{2} I \omega^2}{\frac{1}{2} m v^2} = \frac{\frac{1}{2} \times \frac{2}{5} MR^2 \omega^2}{\frac{1}{2} MR^2 \omega^2} = \frac{2}{5}$$

from (1) and (2)

17. Since the inclined plane is frictionless, then there will be no rolling and the mass will only slide down. Hence acceleration $a = g \sin \theta$ is same for solid sphere, hollow sphere and ring.

$$a = \frac{g \sin \theta}{\left(1 + \frac{K^2}{R^2}\right)}$$

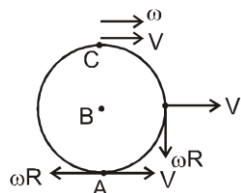
18. In case of pure rolling bottommost point is the instantaneous centre of zero velocity.



Velocity of any point on the disc, $v = r\omega$, where r is the distance of point from O.

$$r_Q > r_C > r_P \quad \therefore \quad v_Q > v_C > v_P$$

Therefore, the correct option is (1).



- 19.

$$\vec{V}_A = V(\hat{i}) + \omega R(-\hat{i}), \quad \vec{V}_B = V\hat{i}, \quad \vec{V}_C = V\hat{i} + \omega R\hat{i}$$

$$\vec{V}_C - \vec{V}_A = 2\omega R\hat{i}$$

$$2[\vec{V}_B - \vec{V}_C] = 2[V(\hat{i}) - V(\hat{i}) - \omega R(\hat{i})] = -2\omega R(\hat{i})$$

Hence $\vec{V}_C - \vec{V}_A = -2(\vec{V}_B - \vec{V}_C)$

so $|\vec{V}_C - \vec{V}_A| = 2|\vec{V}_B - \vec{V}_C|$

$$\vec{V}_C - \vec{V}_B = \omega R(\hat{i})$$

$$\vec{V}_B - \vec{V}_A = \omega R(\hat{i})$$

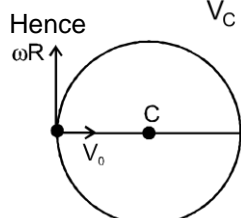
$$\vec{V}_C - \vec{V}_B = \vec{V}_B - \vec{V}_A$$

Hence $\vec{V}_C - \vec{V}_A = 2\omega R(\hat{i})$

$$\vec{V}_C - \vec{V}_B = \vec{V}_B - \vec{V}_A$$

$$\vec{V}_C - \vec{V}_A = 2(\vec{V}_B)$$

$$4\vec{V}_B = 4V(\hat{i}) = 4\omega R(\hat{i})$$



- 20.

For pure rolling $\omega R = u_0$, $u = \sqrt{v_0^2 + (\omega R)^2} = (v_0 \sqrt{2})$

21. Since the two bodies have same mass and collide head-on elastically, the linear momentum gets interchanged.

Hence just after the collision 'B' will move with velocity ' v_0 ' and 'A' becomes stationary but continues to

rotate at the same initial angular velocity $\left(\frac{v_0}{R}\right)$. Hence, after collision.

$$(K.E.)_B = \frac{1}{2}mv_0^2 \text{ and } (K.E.)_A = \frac{1}{2}I\omega^2 = \frac{1}{2}\left(\frac{2}{3}mR^2\right) \cdot \left(\frac{v_0}{R}\right)^2 \Rightarrow \frac{(K.E.)_B}{(K.E.)_A} = \frac{3}{2} \quad \text{Hence (4).}$$

Note : Sphere 'B' will not rotate, because there is no torque on 'B' during the collision as the collision is head-on.

22. $a = \left(\frac{g \sin \theta}{1 + \frac{k^2}{R^2}} \right)$ For solid sphere $\Rightarrow I_{cm} = \frac{2}{5}mk^2 \Rightarrow k_s = R\sqrt{\frac{2}{5}}$

For hollow sphere $= \frac{2}{3}mR^2 = mk^2 \Rightarrow k_H = r\sqrt{\frac{2}{3}}$

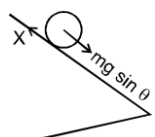
So, $k_s < k_H$ then $a_s > a_H$ (so speed of solid sphere is greater than hollow sphere)

23. $a = \left(\frac{g \sin \theta}{1 + \frac{k^2}{R^2}} \right)$

For solid sphere $\Rightarrow I_{cm} = \frac{2}{5}mk^2 \Rightarrow k_s = R\sqrt{\frac{2}{5}}$

For hollow sphere $= \frac{2}{3}mR^2 = mk^2 \Rightarrow k_H = r\sqrt{\frac{2}{3}}$

So, $k_s < k_H$ then $a_s > a_H$ (so speed of solid sphere is greater than hollow sphere)



24. $mg \sin \theta - f = ma$
 $\frac{mg \sin \theta - f}{m}$

$a = \frac{mg \sin \theta - f}{m}$. a is equal for each body so all the object will reach at same time.

25. Let velocity of c.m. of sphere be v . The velocity of the plank $= 2v$.

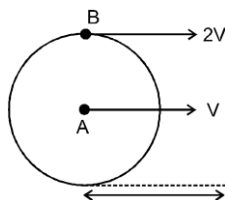
Kinetic energy of plank $= \frac{1}{2} \times m \times (2v)^2 = 2mv^2$

Kinetic energy of cylinder $= \frac{1}{2}mv^2 + \frac{1}{2} \left(\frac{1}{2}mR^2\omega^2 \right) = \frac{1}{2}mv^2 \left(1 + \frac{1}{2} \right) = \frac{3}{2} \cdot \frac{1}{2}mv^2$

$\therefore \frac{\text{K.E. of plank}}{\text{K.E. of sphere}} = \frac{\frac{2mv^2}{3}}{\frac{1}{2}mv^2} = \frac{8}{3}$

26. The horizontal shift of end x will be double the shift of centre of spool. Hence centre travels by $\frac{S}{2}$.

Rigid Body Dynamics



27.

When A point travels ℓ distance then B point 2ℓ so, 2ℓ length of string passes through the hand of the boy

SECTION (I)

1. Total KE = $\frac{1}{2} MV^2 + \frac{1}{2} I\omega^2 = \frac{3}{4} MV^2$

$$\Delta KE = \frac{3}{4} M (4V^2 - V^2) = \frac{9}{4} MV^2$$

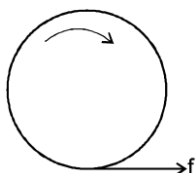
2. $a = \frac{g \sin \theta}{1 + \left(\frac{K}{R}\right)^2} \Rightarrow K (\text{solid sphere}) = \sqrt{\frac{2}{5}} R \Rightarrow K (\text{solid cylinder}) = \frac{R}{\sqrt{2}} \Rightarrow \frac{a_{ss}}{a_{sc}} = \frac{15}{14}$

3. Both spheres reach the ground due to vertical component of velocity. As initial component of velocity of both spheres is zero, therefore both will reach the earth simultaneously. The time taken being given by:

$$h = u_{yt} + \frac{1}{2} gt^2 = 0 + \frac{1}{2} gt^2 \Rightarrow t = \sqrt{\frac{2h}{g}}$$

4. There is no relative motion between sphere and plank so friction force is zero then no any change in motion of sphere and plank.

5. Due to linear velocity body will move forward before pure rolling.

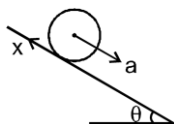


6.

Friction will act in forward direction so body will always move in forward direction.

7. Disc in pure rolling and external force zero after smooth surface pure rolling continue.

8. $mg \sin \theta$ component is always down the plane whether it is rolling up or rolling down. Therefore, for no slipping, sense of angular acceleration should also be same in both the cases. Therefore, force of friction f always act upwards.



9.

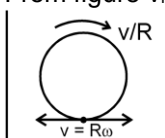
Torque about COM

$$f \cdot R = I \cdot \alpha \quad (a = \alpha R) \Rightarrow F \cdot R = \frac{mR^2}{2} a = \left(\frac{mR^2}{2} \cdot R \right) \Rightarrow \left(f = \frac{ma}{2} \right)$$

10.

As the disc is in combined rotation and translation, each point has a tangential velocity and a linear velocity in the forward direction.

From figure v_{net} (for lowest point) = $v - R\omega = v - v = 0$ and Acceleration = $\frac{v^2}{R} + 0 = \frac{v^2}{R}$



(Since linear speed is constant). Hence (4).

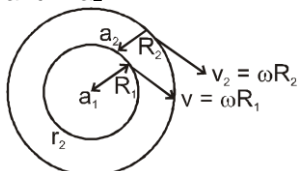
Rigid Body Dynamics

11. When a body rolls down without slipping along an inclined plane of inclination θ , it rotates about a horizontal axis through its centre of mass and also its centre of mass moves. Therefore, rolling motion may be regarded as a rotational motion about an axis through its centre of mass plus a translational motion of the centre of mass. As it rolls down, its loss in gravitational potential energy provided translational energy due to frictional force is converted into rotational energy.

Note : In fact, friction is needed to cause the body to roll. However the rolling friction is so small that we can use conservation of mechanical energy.

12. $ma_1 = \frac{mv_1^2}{R_1}$ (i)

and $ma_2 = \frac{mv_2^2}{R_2}$ (ii)



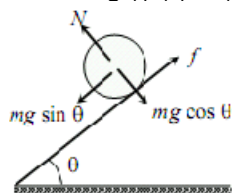
and $\frac{F_1}{F_2} = \frac{ma_1}{ma_2} = \frac{R_2}{mR_2^2\omega^2}$ $\therefore \frac{F_1}{F_2} = \frac{R_1}{R_2}$

13. $mg \sin \theta - f = ma_{CM}$ (i)

$f.R = I\alpha$ (ii)

$a_{CM} = R\alpha$ (iii)

On solving (i), (ii) & (iii)



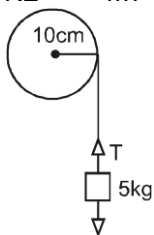
$$a_{CM} = \frac{g \sin \theta}{1 + \frac{I}{MR^2}}$$

14. $a = (g \tan \theta)$ so net force along the inclined plane is zero so it will continue in pure rolling with constant angular velocity.

SECTION (J)

1. As the inclined plane is smooth, the sphere can never roll rather it will just slip down. Hence, the angular momentum remains conserved about any point on a line parallel to the inclined plane and passing through the centre of the ball.

2. $KE = \frac{1}{2} mv^2 (1 + 1) = mv^2 = 0.4 \times 0.1^2 = 4 \times 10^{-3}$.



3. $50 - T = 5a$ (1)
 $TR = I\alpha = Ia/R$ (2)

Rigid Body Dynamics

$$Ia = TR^2$$

$$\text{Now, } 5 = \frac{1}{2} a \times 10 \times 10 \quad \text{so } a = \frac{1}{10} = 0.1 \text{ m/sec}^2$$

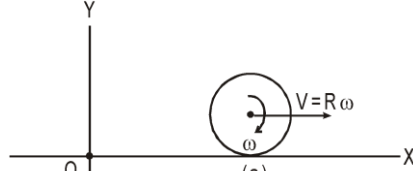
$$\text{So, } 50 - T = 0.5$$

$$\text{So, } T = 50 - 0.5 = 49.5$$

$$\text{So, } I \times 0.1 = \frac{49.5}{10 \times 10}$$

$$\text{So, } I = 4.95 \text{ kg m}^2 \quad \text{None of the answer given.}$$

4. From the theorem –

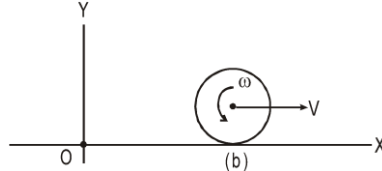


$$L_0 = L_{\text{com}} + M (\vec{r} \times \vec{V}) \quad \dots\dots(1)$$

We may write

Angular momentum about O = Angular momentum about COM + Angular momentum of COM about origin

$$\therefore L_0 = I\omega + MRV = \frac{1}{2} MR^2 \omega + MR(R\omega)$$

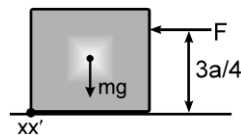


$$= \frac{3}{2} MR^2 \omega$$

Note that in this case both the terms in equation (1) i.e. \vec{L}_{com} and $M(\vec{r} \times \vec{V})$ have the same direction \otimes . That is why we have used $L_0 = I\omega + MRV$. We will use $L_0 = I\omega - MRV$ if they are in opposite directions shown in figure (2).

5. As the inclined plane is smooth, the sphere can never roll rather it will just slip down. Hence, the angular momentum remains conserved about any point on a line parallel to the inclined plane and passing through the centre of the ball.

SECTION (K)

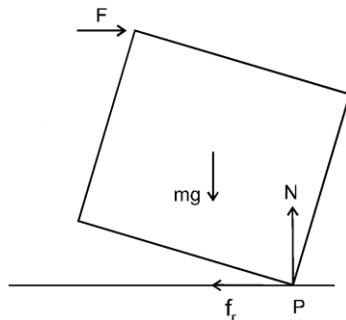


1. For toppling about edge xx' _____

$$F_{\text{min.}} \frac{3a}{4} = mg \frac{a}{2} \quad \Rightarrow \quad F_{\text{min.}} = \frac{2mg}{3}$$

2. At the critical condition, normal reaction N will pass through point P. In this condition $\tau_N = 0 = \tau_{\text{fr}}$ (About P) the block will topple when

Rigid Body Dynamics

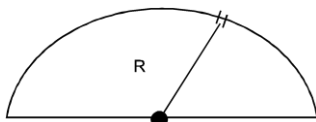


$$\tau_F > \tau_{mg}$$

$$\text{or } FL > (mg) \frac{L}{2} \quad \therefore \quad F > mg / 2$$

EXERCISE # 2

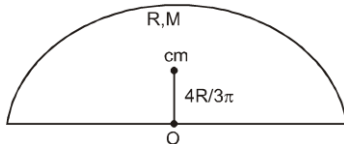
1.



by parallel axis theorem $I = I_{cm} + md^2$

$$M r^2 = I_{CM} + M \left(\frac{2R}{\pi} \right)^2 \Rightarrow I_{CM} = M r^2 \left(1 - \frac{4}{\pi^2} \right)$$

2.



$$I_0 = I_{CM} + M d^2 \Rightarrow \frac{1}{2} M R^2 = I_{CM} + M \left(\frac{4R}{3\pi} \right)^2 \Rightarrow I_{CM} = M R^2 \left(\frac{1}{2} - \frac{16}{9\pi^2} \right)$$

3.

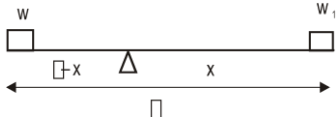
Mass of the ring $M = \rho L$

Let R be the radius of the ring. Then $L = 2\pi R$ or $R = \frac{L}{2\pi}$

Moment of inertia about an axis passing through O , and parallel to XX' will be $I_0 = \frac{1}{2} M R^2$
Therefore, moment of inertia about XX' (from parallel axis theorem) will be given by :

$$I_{XX'} = \frac{3}{2} (\rho L) \left(\frac{L^2}{4\pi^2} \right) = \frac{3\rho L^3}{8\pi^2}$$

4.



weight of object = w

$$w (\ell - x) = w_1 x \quad \dots\dots\dots (i)$$

If weight is kept in another pan then :

$$w_2 (\ell - x) = w x \quad \dots\dots\dots (ii)$$

By (i) & (ii)

$$\frac{w}{w_2} = \frac{w_1}{w} \Rightarrow w^2 = w_1 w_2 \Rightarrow w = \sqrt{w_1 w_2}$$

5.

key Idea : The net moment about point of contact between ground and ladder should be zero. Let (as shown in figure) AB be a ladder and F be the horizontal force to keep it from slipping. w is the weight of man. Suppose N_1 and N_2 be normal reactions of ground and wall respectively.

Rigid Body Dynamics

In horizontal equilibrium,

$$N_1 = F$$

In vertical equilibrium,

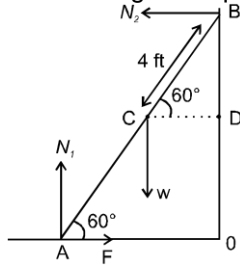
$$N_1 = w$$

Taking moments about A;

Clockwise torque = Anticlockwise torque $N_1 \times CD = N_2 \times OB$ but in $\triangle AOB$, $\sin 60^\circ = \frac{OB}{AB}$

In $\triangle AOB$, $\cos 60^\circ = \frac{CD}{BC} \Rightarrow CD = BC \cos 60^\circ$

Substituting in Eq.(i), we have $N_1 \times BC \cos 60^\circ = N_2 \times AB \sin 60^\circ$



$$\Rightarrow w \times BC \times \frac{1}{2} = F \times AB \times \frac{\sqrt{3}}{2} \quad \text{Given : } w = 150 \text{ pounds, } AB = 20 \text{ mtr., } BC = 4 \text{ mtr.}$$

$$\therefore 150 \times 4 \times \frac{1}{2} = F \times 20 \times \frac{\sqrt{3}}{2} \Rightarrow F = \frac{150 \times 4 \times \sqrt{3}}{20 \times 3} = 17.3 \text{ pound}$$

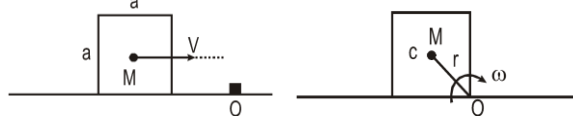
6. Net external torque on the system is zero. Therefore, angular momentum is conserved.
Forces acting on the system are only conservative. Therefore, total mechanical energy of the system is also conserved.

7. $\vec{\tau} \times \vec{L}$ then $\vec{\tau} \parallel \vec{L}$ so $|\vec{L}|$ may increase

8. Here, $u = V_0$, $\omega_0 = \frac{V_0}{2R}$ At pure rolling $V = V_0 - \left(\frac{F_f}{m}\right)t$

$$\& \quad \frac{V}{R} = -\frac{V_0}{2R} + \left(\frac{F_f}{mR}\right)t \quad (\text{In pure rolling } V = R\omega) \quad \left(\alpha = \frac{\tau}{I} = \frac{F_f R}{mR^2}\right)$$

$$\Rightarrow V_0 - V = V + \frac{V_0}{2} \Rightarrow 2V = \frac{V_0}{2} \Rightarrow V = \frac{V_0}{4} \quad \text{Ans.}$$



9. Net torque about O is zero.

Therefore, angular momentum (L) about point O will be conserved,

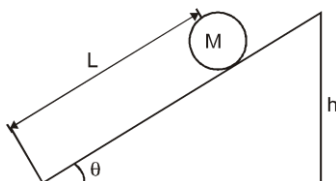
$$\text{or } L_i = L_f$$

$$MV \left(\frac{a}{2}\right) = I_O \omega = (I_{com} + Mr^2)\omega = \left\{ \left(\frac{Ma^2}{6}\right) + M\left(\frac{a^2}{2}\right) \right\} \omega = \frac{2}{3} Ma^2 \omega \Rightarrow \omega = \frac{3V}{4a}$$

10. The linear acceleration of centre of mass will be $a = \frac{F}{m}$ wherever the force is applied. hence, the acceleration will be same whatever the value of h may be

11. The situation is shown in the figure.

Rigid Body Dynamics



Potential energy of cylinder at the top will be converted into rotational kinetic energy and translational kinetic energy. So, energy conservation gives,

$$Mgh = \frac{1}{2}mv^2 + \frac{1}{2}I\omega^2 = \frac{1}{2}mv^2 + \frac{1}{2} \frac{MR^2}{2} \frac{v^2}{R^2} \left(\because I_{\text{cylinder}} = \frac{MR^2}{2} \right) \quad \text{So,} \quad Mgh = \frac{1}{2}Mv^2 + \frac{1}{4}Mv^2$$

$$\text{or} \quad Mgh = \frac{3}{4}Mv^2 \quad \text{or} \quad v^2 = \frac{4}{3}gh \quad \text{or} \quad v = \sqrt{\frac{4}{3}gh}$$

12. Mass of disc (X), $m_X = \pi R^2 t \rho$
Where ρ = density of material of disc

$$\therefore I_X = \frac{1}{2} m_X R^2 = \frac{1}{2} \pi R^2 t \rho R^2$$

$$I_X = \frac{1}{2} \pi \rho R^4 \quad \dots\dots(i) \quad \text{Again mass of disc (Y)}$$

$$m_Y = \pi (4R)^2 \frac{t}{4} \rho = 4\pi R^2 t \rho \quad \text{and} \quad I_Y = \frac{1}{2} m_Y (4R)^2 = \frac{1}{2} 4\pi R^2 t \rho \cdot 16R^2$$

$$\frac{I_Y}{I_X} = \frac{32\pi t \rho R^4}{\frac{1}{2} \pi t \rho R^4} = 64$$

$$\Rightarrow I_Y = 32\pi t \rho R^4 \quad \dots\dots(ii) \quad \therefore I_Y = 64 I_X$$

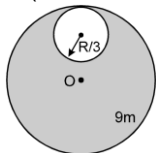
13. Mass of the whole disc = $4M$

$$\text{Moment of inertia of the disc about the given axis} = \frac{1}{2} (4M)R^2 = 2MR^2$$

$$\therefore \text{Moment of inertia of quarter section of the disc} = \frac{1}{4} (2MR^2) = \frac{1}{2} MR^2$$

These type of questions are often asked in objective. Students generally err in taking mass of the whole disc. They take it M instead of $4M$.

14. $I_0 = I_1 - I_2$ where I_1 = (M.I. of full disc about O)
 I_2 (M.I. of small removed disc about O) since mass \propto area



$$\frac{\text{mass of cut disc}}{\text{mass of total}} = \frac{\frac{R^2}{9}}{R^2} = \frac{1}{9} \quad \therefore \text{mass of cut disc} = m$$

$$\therefore I_0 = \frac{(9m)R^2}{2} - m \left[\frac{\left(\frac{R}{3}\right)^2}{2} + \left(\frac{2R}{3}\right)^2 \right] \quad (\text{by theorem of parallel axis.})$$

$$= \frac{9mR^2}{2} - mR^2 \left[\frac{1}{18} + \frac{4}{9} \right] = \frac{9mR^2}{2} - \frac{5mR^2}{6} = \frac{12mR^2 - 5mR^2}{6} = \frac{7mR^2}{6}$$

15. $\frac{2}{5} MR^2 = \frac{1}{2} Mr^2 + Mr^2 \therefore \frac{2}{5} MR^2 = \frac{3}{2} Mr^2$

$$r^2 = \frac{4}{15} R^2 \quad \Rightarrow \quad r = \frac{2R}{\sqrt{15}}$$

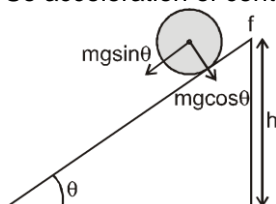
Rigid Body Dynamics

16. If torque external = 0, then angular momentum = constant = $I\omega$

17. The acceleration of centre of mass of either cylinder

$$a = \frac{g \sin \theta}{1 + \frac{K^2}{R^2}} \quad \text{where } K \text{ is radius of gyration.}$$

So acceleration of centre of hollow cylinder



is less than that of solid cylinder.

Hence time taken by hollow cylinder will be more.

So statement-1 is wrong. **Ans. (4)**

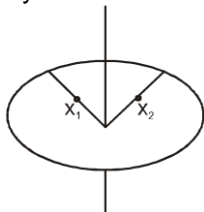
18. (1) Since there is no resultant external force, linear momentum of the system remains constant.

(2) Kinetic energy of the system may change.

(3) Angular momentum of the system may change as in case of couple, net force is zero but torque is not zero. Hence angular momentum of the system is not constant.

(4) Potential energy may also change.

19. By conservation of angular momentum



$$MR^2 \omega = \left(MR^2 + \frac{M}{8} \frac{9R^2}{25} + \frac{Md^2}{8} \right) \frac{8\omega}{9} \Rightarrow R^2 = \left(\frac{200R^2 + 9R^2 + 25d^2}{8 \times 25} \right) \frac{8}{9}$$

$$225 R^2 - 209 R^2 = 25 d^2$$

$$\frac{16R^2}{25} \Rightarrow d = \frac{4R}{5}$$

20. Moment of Inertia about the shortest side BC is greater than the other two sides

$$I_{BC} > I_{AB}$$

21. Conserving the angular momentum :

$$mua = \left[\frac{m(a^2 + 4a^2)}{12} + \frac{5}{4} ma^2 \right] \omega \Rightarrow \omega = \frac{3}{5} \frac{u}{a} \quad \text{Ans.}$$

22. By conservation of angular momentum about hinge O.

$$L = I \omega$$

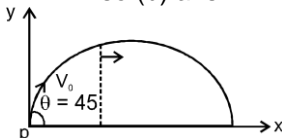
$$mv \frac{d}{2} = \left[\frac{Md^2}{12} + m \left(\frac{d}{2} \right)^2 \right] \omega \Rightarrow \frac{mvd}{2} = \left(\frac{md^2}{2} + \frac{md^2}{4} \right) \omega$$

$$\frac{mvd}{2} = \frac{3}{4} md^2 \omega \Rightarrow \frac{2}{3} \frac{v}{d} = \omega$$

23. $L = Pr$ so $\log = \log P + \log r$

$$y = x + \log r$$

so (b) ans.



24.

$$x = v_0 \cos 45^\circ \times t = \frac{v_0 t}{\sqrt{2}} \Rightarrow \tau = mgx = \frac{mgv_0 t}{\sqrt{2}} = \frac{dL}{dt} \Rightarrow L = \frac{mgv_0}{\sqrt{2}} \int_0^{v_0/g} t \, dt = \frac{mv_0^3}{2\sqrt{2}g}$$

25. In rolling without slipping, total energy of ball is the sum of its translational and rotational energy. Kinetic energy of rotation is

$$K_{\text{rot}} = \frac{1}{2} I \omega^2 = \frac{1}{2} M K^2 \frac{v^2}{R^2} \text{ where } K \text{ is radius of gyration.}$$

$$\text{Kinetic energy of translation is } K_{\text{trans.}} = \frac{1}{2} M v^2$$

$$\text{Thus, total energy } E = K_{\text{rot.}} + K_{\text{trans.}} = \frac{1}{2} M K^2 \frac{v^2}{R^2} + \frac{1}{2} M v^2 = \frac{1}{2} M v^2 \left(\frac{K^2}{R^2} + 1 \right) = \frac{1}{2} \frac{M v^2}{R^2} (K^2 + R^2)$$

$$\frac{K_{\text{rot.}}}{K_{\text{trans.}}} = \frac{\frac{1}{2} M K^2 \frac{v^2}{R^2}}{\frac{1}{2} M v^2 \left(\frac{K^2}{R^2} + 1 \right)} = \frac{K^2}{K^2 + R^2}$$

Hence,

26. As no external torque is applied to the system, the angular momentum of the system remains conserved.

$$\therefore L_i = L_f \text{ According to given problem,}$$

$$I_t \omega_i = (I_t + I_b) \omega_f$$

$$\omega_f = \frac{I_t \omega_i}{(I_t + I_b)}$$

$$\text{or} \dots\dots\dots(i)$$

$$\text{Initial energy, } E_i = \frac{1}{2} I_t \omega_i^2 \dots\dots\dots(ii)$$

$$\text{Final energy, } E_f = \frac{1}{2} (I_t + I_b) \omega_f^2 \dots\dots\dots(iii)$$

Substituting the value of ω_f from equation (i) in equation (iii) we get

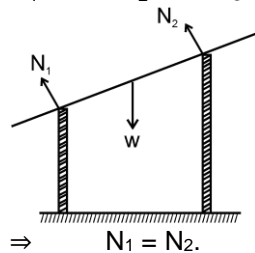
$$\begin{aligned} \text{Final energy, } E_f &= \frac{1}{2} (I_t + I_b) \left(\frac{I_t \omega_i}{I_t + I_b} \right)^2 \\ &= \frac{1}{2} \frac{I_t^2 \omega_i^2}{(I_t + I_b)} \dots\dots\dots(iv) \end{aligned}$$

$$\text{Loss of energy, } \Delta E = E_i - E_f = \frac{1}{2} I_t \omega_i^2 - \frac{1}{2} \frac{I_t^2 \omega_i^2}{(I_t + I_b)} \quad (\text{Using (ii) and (iv)})$$

$$= \frac{\omega_i^2}{2} \left(I_t - \frac{I_t^2}{(I_t + I_b)} \right) = \frac{\omega_i^2}{2} \left(\frac{I_t^2 + I_b I_t - I_t^2}{(I_t + I_b)} \right) = \frac{1}{2} \frac{I_b I_t}{(I_t + I_b)} \omega_i^2$$

27. Balancing torque about the centre of the rod :

$$N_1 \cdot \frac{\ell}{4} - N_2 \cdot \frac{\ell}{4} = 0$$



EXERCISE # 3 PART - I

3. Mass of the disc = 9M

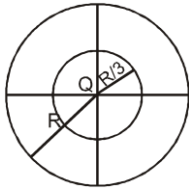
Rigid Body Dynamics

Mass of removed portion of disc = M

The moment of inertia of the complete disc about an axis passing through its centre O and perpendicular

to its plane is $I_1 = \frac{9}{2}MR^2$

Now, the moment of inertia of the disc with removed portion $I_2 = \frac{1}{2}M\left(\frac{R}{3}\right)^2 = \frac{1}{18}MR^2$



Therefore, moment of inertia of the remaining portion of disc about O is

$$I = I_1 - I_2 = \frac{9}{2}MR^2 - \frac{MR^2}{18} = \frac{40MR^2}{9}$$

Rigid Body Dynamics

4. When angular acc. (α) is zero than torque on the wheel becomes zero

$$\theta(t) = 2t^3 - 6t^2$$

$$\frac{d\theta}{dt} = 6t^2 - 12t \quad \Rightarrow \quad \frac{d^2\theta}{dt^2} = 12t - 12 = 0 \quad \Rightarrow \quad t = 1 \text{ Sec.}$$

6. It's always in axial direction so

7. at maximum compression the solid cylinder will stop

so loss in K.E. of cylinder = gain in P.E. of spring

$$\Rightarrow \frac{1}{2}mv^2 + \frac{1}{2}I\omega^2 = \frac{1}{2}kx^2 \Rightarrow \frac{1}{2}mv^2 + \frac{1}{2} \frac{mR^2}{2} \left(\frac{v}{R}\right)^2 = \frac{1}{2}kx^2$$

$$\Rightarrow \frac{3}{4}mv^2 = \frac{1}{2}kx^2 \quad \Rightarrow \quad \frac{3}{4} \times 3 \times (4)^2 = \frac{1}{2} \times 200 \times x^2$$

$$\Rightarrow \frac{36}{100} = x^2 \quad \Rightarrow \quad x = 0.6 \text{ m}$$

8. $F_1x + F_2x = F_3x \quad \Rightarrow \quad F_3 = F_1 + F_2$

9. using angular momentum conservation

$$L_i = 0$$

$$L_t = mvR - I\omega$$

$$mvR = I\omega$$

$$\omega = \left(\frac{1}{2}\right)$$

$$(v + \omega R)t = 2\pi R$$

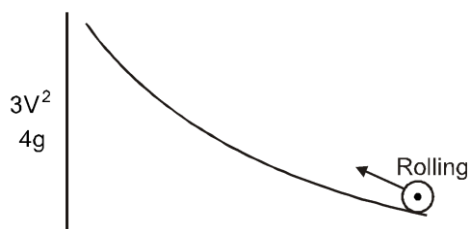
$$\left(1 + \frac{1}{2} \times 2\right) = 2\pi \times 2$$

$$t = 2\pi \text{ sec.}$$

10. $I = I_{cm} + md^2$

d is maximum for point B so

I_{max} about B

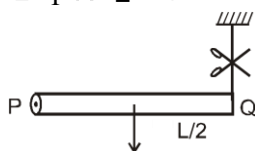


- 11.

$$\frac{1}{2}I\omega^2 + 0 + \frac{1}{2}mv^2 = mg \times \frac{3v^2}{4g}$$

$$\frac{1}{2}I\omega^2 = \frac{3}{4}mv^2 - \frac{1}{2}mv^2 = \frac{mv^2}{2} \left(\frac{3}{2} - 1\right)$$

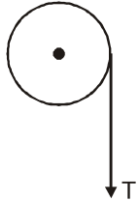
$$\frac{1}{2}I \frac{V^2}{R^2} = \frac{mv^2}{4} \quad \Rightarrow \quad I = \frac{1}{2}mR^2 \text{ Disc}$$



- 12.

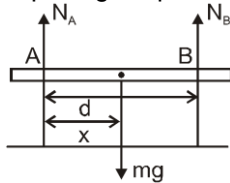
$$I = mg \frac{L}{2} = I\alpha = \frac{mL^2}{3} \alpha \quad \Rightarrow \quad a = \alpha = \frac{3g}{2L}$$

13. $(T) \times (R) = \left(\frac{MR^2}{2} \right) (\alpha)$



$$T = \left(\frac{MR}{2} \right) (\alpha) = \left(\frac{50 \times 0.5}{2} \right) (2 \times 2\pi) = 157\text{N}$$

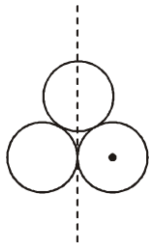
14. Equating torque about center of mass



$$N_A x = N_B (d-x)$$

$$N_A + N_B = mg \quad \Rightarrow \quad \text{Solving } N_A = \frac{W(d-x)}{d}$$

15. $I_{\text{diameter}} = \frac{2}{3} MR^2$



$$I_{\text{tangential}} = \frac{2}{3} MR^2 + MR^2 = \frac{5}{3} MR^2 \quad \therefore \text{So } I_{\text{total}} = \frac{2}{3} MR^2 + \left(\frac{5}{3} MR^2 \right) \times 2 = 4MR^2 = \frac{12}{3} MR^2 = 4MR^2$$

16. $\text{K.E.} = \frac{1}{2} I \omega^2$

I is min. about the centre of mass

$$\text{So. } (m_1)(x) = (m_2)(L-x)$$

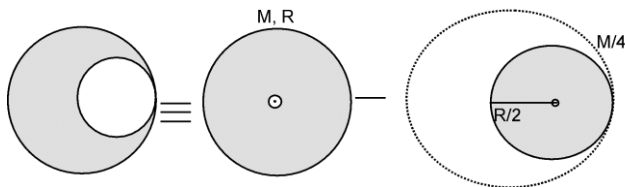
$$x = \frac{m_2 L}{m_1 + m_2}$$

17. If \dot{L} = constant then $\vec{\tau} = 0$

$$\text{so } \vec{r} \times \vec{F} = 0 \Rightarrow \text{should be parallel to } \vec{r} \text{ so coefficient should be in same ratio. So } \frac{\alpha}{2} = \frac{3}{-6} = \frac{6}{-12}$$

So $\alpha = -1$ **Ans (4)**

Rigid Body Dynamics



18.

$$I_1 = \frac{MR^2}{2}$$

$$I_2 = \frac{\left(\frac{M}{4}\right)\left(\frac{R}{2}\right)^2}{2} + \left(\frac{M}{4}\right)\left(\frac{R}{2}\right)^2 = \frac{3MR^2}{32} \Rightarrow I_{\text{net}} = I_1 - I_2 = \frac{MR^2}{2} - \frac{3MR^2}{32} = \frac{13MR^2}{32} \quad \text{So, answer is 3.}$$

19. Time does not depend on mass, else

$$t \propto \sqrt{1 + \frac{k^2}{R^2}} \Rightarrow \frac{k^2}{R^2} \text{ is least for sphere and hence least time is taken by sphere}$$

20. The angular speed of disc increases with time, and hence centripetal acceleration

$$\text{also } a_{\text{net}} = \sqrt{a_t^2 + a_c^2}$$

$$a_c = \frac{v^2}{R}$$

v = tangential speed

R = Radius = 0.5 m

$$V = 2 \text{ m/s at } t = 2 \Rightarrow a_c = 8 \text{ m/s}^2; a_t = R\alpha = (0.5)(2) \Rightarrow a_{\text{net}} = \sqrt{8^2 + 1^2} \simeq 8$$

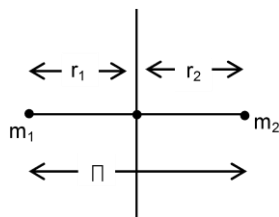
21. $KE_A = KE_B$

$$\frac{1}{2} I_A \omega_A^2 = \frac{1}{2} I_B \omega_B^2 \Rightarrow \text{since } I_B > I_A \text{ so } \omega_B < \omega_A$$

$$\frac{1}{2} L_A \omega_A = \frac{1}{2} L_B \omega_B \Rightarrow L_B > L_A \quad \text{Ans.}$$

22. KE of sphere = $\frac{1}{2} \left(\frac{2}{5} mR^2 \right) \omega^2 = \frac{1}{5} mR^2 \omega^2$

$$\text{KE of cylinder} = \frac{1}{2} \left(\frac{mR^2}{2} \right) (2\omega)^2 = mR^2 \omega^2 \quad \text{So, } \frac{KE_{\text{sphere}}}{KE_{\text{cylinder}}} = \frac{1}{5} \quad \text{Ans.}$$



23.

$$I = m_1 r_1^2 + m_2 r_2^2 = m_1 \left(\frac{m_2}{m_1 + m_2} \ell \right)^2 + m_2 \left(\frac{m_1}{m_1 + m_2} \ell \right)^2 = \frac{m_1 m_2 (m_1 + m_2) \ell^2}{(m_1 + m_2)^2} = \frac{m_1 m_2 \ell^2}{(m_1 + m_2)} \quad \text{Ans.}$$

Rigid Body Dynamics

24. $KE_t = \frac{1}{2}mV^2$

$$KE_{\text{rotation}} = \frac{1}{2}I_{\text{cm}}\omega^2 = \frac{1}{2}\left(\frac{2}{5}MR^2\right)\left(\frac{V}{R}\right)^2 = \frac{1}{5}mV^2 \Rightarrow \frac{KE_t}{KE_t + KE_r} = \frac{\frac{1}{2}mV^2}{\frac{1}{2}mV^2 + \frac{1}{5}mV^2} = \frac{5}{7}$$

25. $\tau_{\text{ext}} = 0$, so Angular momentum will remain conserved.

26. Measured diameter of ball = Main scale reading + Circular scale reading \times least count
 $= 5 \text{ mm} + (25) \times (0.01 \text{ mm}) = 5.25 \text{ mm}$
 Actual diameter = measured diameter – zero error = $(5.25 \text{ mm}) - (-0.04 \text{ mm}) = 5.29 \text{ mm}$

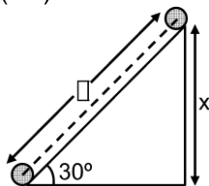
27. $\omega_0 = 3 \text{ rpm} = 3 \times \frac{2\pi}{60} \text{ rad/sec} = \frac{\pi}{10}$
 $\omega^2 = \omega_0^2 + 2\alpha\theta$

$$0^2 = \left(\frac{\pi}{10}\right)^2 + 2(\alpha)(2\pi \times 2\pi) \Rightarrow \alpha = -\frac{1}{800} \text{ rad/sec}^2$$

$$I = \frac{mR^2}{2} = \frac{(2)\left(\frac{4}{100}\right)^2}{2} = \frac{16}{10^4} \Rightarrow \tau = I\alpha = \left(\frac{16}{10^4}\right) \times \left(-\frac{1}{800}\right) = -2 \times 10^{-6} \text{ N.m}$$

28. work done = ΔKE

$$(KE)_i = \frac{1}{2}I\omega^2 + \frac{1}{2}mv^2 = \frac{3}{4}mv^2 = \frac{3}{4} \times 100 \times (20 \times 10^{-2})^2 = \frac{3}{4} \times 100 \times 400 \times 10^{-4} = 3 \text{ J}$$



29.

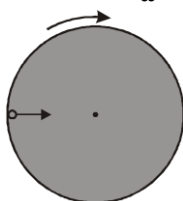
By energy conservation $\frac{1}{2}mv^2 \left(1 + \frac{K^2}{R^2}\right) = mgx = mg\ell \sin\theta$

$$\text{So } \ell = \frac{v^2(1 + K^2/R^2)}{2g\sin\theta} \Rightarrow L = \frac{(4)^2 \times \left(1 + \frac{1}{2}\right)}{2 \times 10 \times \frac{1}{2}} = 2.4 \text{ meter}$$

PART - II

1. $\frac{1}{2}I\omega^2 = mgh$

$$\frac{1}{2}\left(\frac{ml^2}{3}\right)\omega^2 = mgh \quad h = \frac{\omega^2 \ell^2}{6g}$$

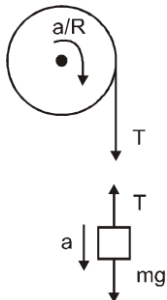


2.

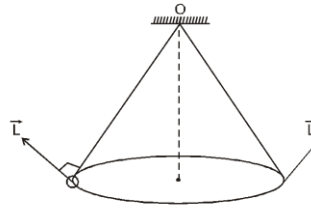
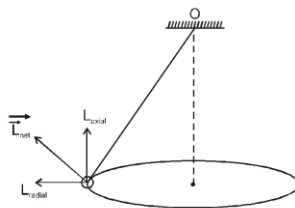
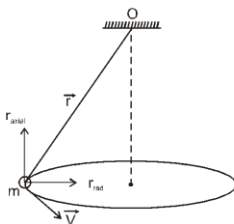
Rigid Body Dynamics

From angular momentum conservation about vertical axis passing through centre. When insect is coming from circumference to center. Moment of inertia first decrease then increase. So angular velocity increase then decrease.

3. To reverse the direction $\int \tau d\theta = 0$ (work done is zero)
 $\tau = (20t - 5t^2) \cdot 2 = 40t - 10t^2$
 $\alpha = \frac{\tau}{I} = \frac{40t - 10t^2}{10} = 4t - t^2 \Rightarrow \omega = \int_0^t \alpha dt = 2t^2 - \frac{t^3}{3}$
 ω is zero at $2t^2 - \frac{t^3}{3} = 0$
 $t^3 = 6t^2 \Rightarrow t = 6 \text{ sec.}$
 $\theta = \int \omega dt = \int_0^6 (2t^2 - \frac{t^3}{3}) dt \Rightarrow \left[\frac{2t^3}{3} - \frac{t^4}{12} \right]_0^6 = 216 \left[\frac{2}{3} - \frac{1}{2} \right] = 36 \text{ rad.}$
 No of revolution $\frac{36}{2\pi}$ Less than 6

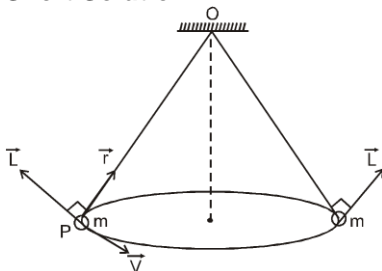


4. $mg - T = ma \dots (1)$
 $T \cdot R = mR^2 \frac{a}{R} \dots (2) \Rightarrow \frac{g}{2} = a$



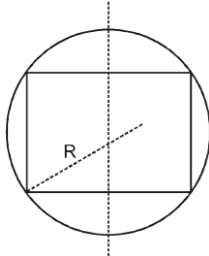
5. Angular momentum of the pendulum about the suspension point 'O' is
 $L = m (\mathbf{r} \times \mathbf{v})$
 Then \mathbf{L} can be resolved into two components, radial component r_{rad} , and axial component r_{axial} . Due to r_{rad} , L will be axial and due to r_{axial} , L will be radially outwards as shown.
 So net angular momentum will be as shown in figure whose value will be constant ($|L| = mv\ell$). But its direction will change as shown in the figure.

Short Solution

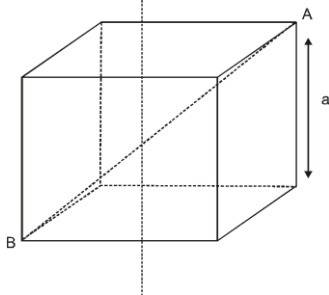


Angular momentum of the pendulum about the suspension point 'O' will have a constant magnitude : $(L) = mv(\ell)$ but its direction will change as shown in the figure.

6. $AB = 2R$
 $a\sqrt{3} = 2R$
 $a = \frac{2R}{\sqrt{3}}$

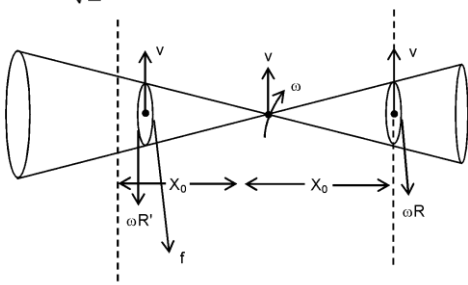


$$\text{Mass of cube} = \frac{M}{\frac{4}{3}\pi R^3} \times \left(\frac{2R}{\sqrt{3}}\right)^3 = \frac{3M}{4\pi R^3} \cdot \frac{8R^3}{3\sqrt{3}} = \frac{2M}{\sqrt{3}\pi}$$



$$\text{Moment of inertia of cube about given axis is} = \frac{ma^2}{6} = \frac{2M}{\sqrt{3}\pi} \cdot \frac{4R^2}{3} \cdot \frac{1}{6} = \frac{4MR^2}{9\sqrt{3}\pi}$$

7. From C to D
 $\vec{L}_0 = mv \left[\frac{R}{\sqrt{2}} + a \right] \hat{k}$ from B to C
 $\vec{L}_0 = mv \left[\frac{R}{\sqrt{2}} + a \right] \hat{k}$ from D to A
 $\vec{L}_0 = \frac{mv}{\sqrt{2}} R (-\hat{k})$ from A to B
 $\vec{L}_0 = \frac{mv}{\sqrt{2}} R (-\hat{k})$



8. At distance x_0 from O $v = \omega R$
 distance less than x_0 $v > \omega R$
 Initially, there is pure rolling at both the contacts. As the cone moves forward slipping at AB will start in forward direction as radius at left contact decreases.

Rigid Body Dynamics

Thus the cone will start turning towards left. As it moves further slipping at CD will start in backward direction which will also turn the cone towards left.

At distance x_0 from O $v = \omega R$

Distance less than X_0 $v > \omega R$

$$I = \frac{M\bar{x}^2}{12} + \frac{MR^2}{4}$$

9.



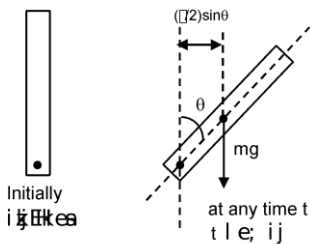
$$= \frac{M\bar{x}^2}{12} + \frac{M}{4} \times \frac{M}{\rho\pi\bar{x}} \Rightarrow M = (\pi R^2 \ell) \rho \Rightarrow \frac{M}{\rho\pi\ell} = R^2$$

$$\frac{dI}{d\ell} = \frac{M}{12}(2\ell) - \frac{M^2}{4\rho\pi}\left(\frac{1}{\ell^2}\right) = 0$$

$$\Rightarrow \frac{\bar{x}}{6} = \frac{M}{4\rho\pi\bar{x}^2}$$

$$\bar{x}^3 = \frac{3M}{2\rho\pi} = \frac{3}{2\rho\pi} \times \pi R^2 \bar{x} \rho$$

$$\Rightarrow \frac{\bar{x}^2}{R^2} = \frac{3}{2} \Rightarrow \frac{\bar{x}}{R} = \sqrt{\frac{3}{2}}$$

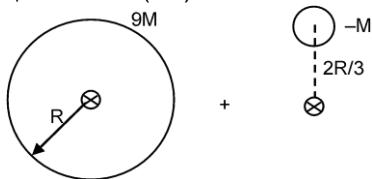


10.

$$mg \sin \theta \frac{\bar{x}}{2} = \frac{m\bar{x}^2}{3} \alpha \Rightarrow \frac{3g}{2\bar{x}} \sin \theta = \alpha$$

11.

$$I_p = I_0 + 7M(3R)^2 = \left(\frac{MR^2}{2} + 6 \left(\frac{MR^2}{2} + M(2R)^2 \right) \right) + 7M(3R)^2 = \frac{181}{2} MR^2$$



12.

[Using negative mass concept]

$$I = \frac{9MR^2}{2} - \left[\frac{M\left(\frac{R}{3}\right)^2}{2} + M\left(\frac{2R}{3}\right)^2 \right] = MR^2 \left[\frac{9}{2} - \frac{1}{18} - \frac{4}{9} \right] = 4MR^2$$

13.

From Dimension analysis $I_0 = kMa^2$

Now for small lamina

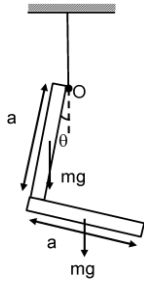
$$I' = k \frac{M\left(\frac{a}{2}\right)^2}{4} = \frac{kMa^2}{16} \Rightarrow I' = \frac{I_0}{16}$$

So moment of inertia of remaining part $I - I' = \frac{15I_0}{16}$

14.

Lets considered mass of each rod is m for equilibrium the torque about point O should be zero.

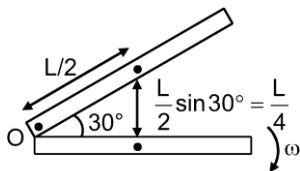
Rigid Body Dynamics



Torque balance about O

$$mg \frac{a}{2} \sin \theta = mg \left(\frac{a}{2} \cos \theta - a \sin \theta \right)$$

$$\tan \theta = \frac{1}{3} \quad \Rightarrow \quad \tan^{-1} \left(\frac{1}{3} \right)$$



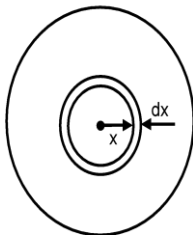
15.

$$\frac{1}{2} I \omega^2 = Mg \frac{L}{4}$$

$$\Rightarrow \quad \frac{1}{2} \frac{ML^2}{3} \omega^2 = Mg \frac{L}{4} \quad \Rightarrow$$

$$\omega^2 = \frac{3g}{2L} = \frac{3 \times 10}{2 \times \frac{1}{2}} = 30$$

$$\Rightarrow \quad \omega = \sqrt{30} \text{ rad/s}$$

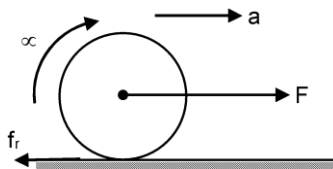


16.

Net torque = \sum Torque on ring

$$\int d\tau = \int_0^R \mu \times \frac{F}{\pi R^2} \times 2\pi x \cdot x dx$$

$$\tau = \frac{2\mu FR}{3}$$



17.

$$F - f_r = ma \quad \dots\dots(1)$$

$$f_r R = I \alpha = \frac{mR^2}{2} \alpha \quad \dots\dots(2)$$

for pure rolling

$$a = \alpha R \quad \dots\dots(3)$$

from (1)(2) and (3)

Rigid Body Dynamics

$$F - \frac{mR\alpha}{2} = m\alpha R$$

$$\Rightarrow F = \frac{3}{2}mR\alpha \Rightarrow \alpha = \frac{2F}{3mR}$$

$$18. \quad 5M_0g\ell - 4M_0g\ell = [2M_0(2\ell)^2 + 5M_0(\ell^2)]\alpha$$

$$M_0g\ell = (13M_0\ell^2)\alpha$$

$$\alpha = \left(\frac{g}{13\ell} \right)$$

$$19. \quad I_0 = (\text{M.I. of A \& B}) + (\text{M.I. of C})$$

$$I_0 = \left(\frac{MR^2}{4} + MR^2 \right) \times 2 + \frac{MR^2}{2} = \frac{5MR^2}{2} + \frac{MR^2}{2} = 3MR^2$$

$$20. \quad \text{Taking torque about the point of contact}$$

$$40 \times [1] = [mr^2 + mr^2]\alpha$$

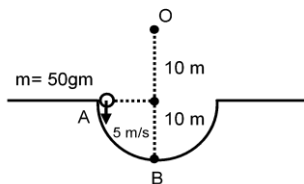
$$40 = 2m \times \frac{1}{4} \alpha \Rightarrow 40 = 2 \times 5 \times \frac{1}{4} \alpha. \quad \therefore \alpha = 16 \text{ rad/s}^2$$

$$21. \quad \vec{\tau} = \vec{r} \times \vec{F} \Rightarrow \tau = rF \sin\theta \Rightarrow 2.5 = 5 \times 1 \times \sin\theta \Rightarrow \theta = 30^\circ$$

$$22. \quad T_0 = \vec{r}_1 \times \vec{F}_1 + \vec{r}_2 \times \vec{F}_2 = (2\hat{i} + 3\hat{j}) \times F(\hat{k}) + 6\hat{j} \times \left(\frac{F}{2}(-\hat{i}) + \frac{F\sqrt{3}}{2}(-\hat{j}) \right)$$

$$= 2F(-\hat{j}) + 3F(\hat{i}) + 3F(\hat{k}) + 0 = (3\hat{i} - 2\hat{j} + 3\hat{k})F$$

$$23. \quad \text{Applying conservation of energy}$$



$$mgR = \frac{1}{2}mV_2^2 - \frac{1}{2}mV_1^2$$

$$V_2 = \sqrt{2gr + V_1^2} = \sqrt{2 \times 10 \times 10 + 25}$$

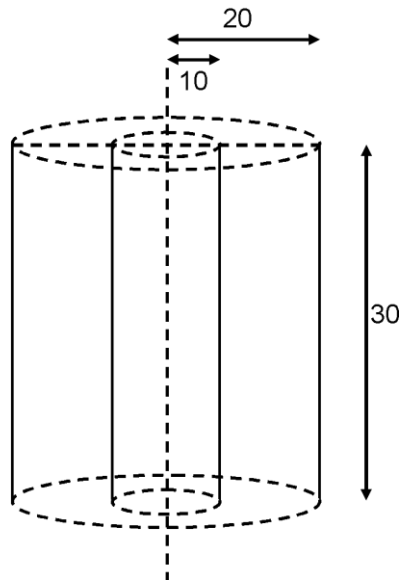
$$V_2 = 15 \text{ m/s}$$

$$L_0 = mV_{Br} = 20 \times 10^{-3} \times 20 \times 15$$

$$L_0 = 6 \text{ kgm}^2/\text{s}$$

$$24. \quad I_x = I_{cm} + mx^2$$

$$I_x = \frac{2}{5}mR^2 + mx^2 \Rightarrow \text{Parabola opening upward}$$



25.

$$\frac{m(20^2 + 10^2)}{2} = mk^2 \Rightarrow K = \sqrt{\frac{400 + 100}{2}} \quad K = \sqrt{250}$$

$$K = 5\sqrt{10} \text{ cm}$$