TOPIC : CHEMICAL EQUILIBRIUM EXERCISE # 1

Section (A)

- 2. At equilibrium all properties solution (i.e. chemical composition of eq. mixture) becomes constant.
- 4. At equilibrium rates of backward and forward reactions become equal.
- 5. Concentration of reactant & product remains const. w.r.t time. And, rate of [AT EQUILIBRIUM] forward reaction (r_f) = rate of backward reaction.
- 7. Molar conc. = $\frac{\text{no. of molar (mole)} O_2}{\text{volume (in l itre)}} = \frac{869}{329} \times 2 = 1.5 \text{ mol/litre}$
- Forward reaction rate (r_i) [A] [B] = K₁ [A] [B] 8. Backward reaction rate $(r_{f}) = K_{h} [C] [D] = K_{2} [C] [D]$ At equilibrium, $r_f = r_h$ \therefore K_1 [A] [B] = K_2 [C] [D] The concentration of reactents & products at equilibrium are related by $\mathsf{K} = \frac{\mathsf{K}_1}{\mathsf{K}_2} = \frac{[\mathsf{C}] \quad [\mathsf{D}]}{[\mathsf{A}] \quad [\mathsf{B}]} \qquad \therefore \qquad \mathsf{K}(\mathsf{K}_c) = \frac{\mathsf{K}_1}{\mathsf{K}_2}$ $\mathsf{K} = \frac{\mathsf{r}_{\mathsf{f}}}{\mathsf{r}_{\mathsf{b}}} \qquad \Rightarrow \qquad 1.5 = \frac{\mathsf{r}_{\mathsf{f}}}{7.5 \times 10^{-4}} \qquad \Rightarrow \qquad \mathsf{r}_{\mathsf{f}} = 1.12 \times 10^{-3}.$ 9. $K_{c} = \frac{[Z]^{2}}{[X]^{2} [Y]^{2}}$ 10. $N_2 + O_2 \implies 2NO$ 11. $K_{p} = \frac{P_{NO}^{2}}{P_{N_{2}}.P_{O_{2}}}$ (i) $2NO \implies N_2 + O_2$ $K'_{p} = \frac{P_{N_{2}}.P_{O_{2}}}{P_{NO}^{2}}$ (ii) From equation (i) and (ii), we have $K'_{p} = \frac{1}{K} = \frac{1}{100} = 0.01$ $K_{1} = \frac{(SO_{3})}{(SO_{2})(O_{2})^{1/2}}$ 13.

$$K_2 = \frac{(SO_2)^4 (O_2)^2}{(SO_3)^4} = \frac{1}{(K_1)^4} \implies K_2 = \frac{1}{(K_1)^4}$$

- **16.** Equilibrium const. is temp. dependent only.
- **18.** Since, K_{p} is temperature dependent only.

20.
$$N_2OH_{(g)} \rightleftharpoons 2NO_{2(g)}$$

 $\Delta n = 2 - 1 = 1, \quad K_p = K_c \text{ (given)}$
We know, $K_p = K_c (RT)^{\Delta n}$
 $1 = RT, \quad T = \frac{1}{.0821} = 12.19 \text{ K}$

21.	Relation between K_{p} and K_{c} is :						
23.	for $K_p = K_c$, $\Delta n = 0$ only option (3) with satisfy this condition.						
24.	For this	s reaction, $K_{c} = \frac{[X]^{4}}{[A]^{4}}$	Y] ⁶ B] ⁵				
	So the	unit of $K_c = \left[\frac{\text{mole}}{\text{litre}}\right]^{(4+6)}$	-(4+5) = m	ole litre-1			
S ECTIO	N (B)						
1.	()	$PCl_5(g) \longrightarrow PCl_3(g)$	+ Cl ₂ (g)				
	t=0						
	t=t _{eq}	1 0 1 - x x	х				
	Total m	noles = $1 + x$					
	Given	$\frac{1-x}{1+x} = 0.4 \qquad \Rightarrow \qquad \qquad$	$x = \frac{3}{7}$		⇒	X _{PCl3} =	$\frac{\frac{3}{7}}{\frac{1+\frac{3}{7}}{7}} = 0.3.$
2.		────────────────────────────────────					I
		0 0	t = 0				
	(3n—x) (n—x) :) (n—x) x x = x	t = teq.				
	n = 2x	$x = \frac{n}{2}$					
6.>	A + E	$B \rightleftharpoons C + D$ $4 4 0$ $4 - 2 4 - 2 2$					
	t = 0	4 4 0	0				
	-	-	2				
	$K_{c} = \frac{2}{2}$	$\frac{\times 2}{\times 2} = 1$					
7.	2P(g)	$+ Q(g) \implies 3R(g)$	+ S(g))			
	t = 0	+ Q(g) \rightleftharpoons 3R(g) 2 2	0	x/2			
	t = teq	2 - x $2 - x/2$	3/2 x	x/2			
		pove, at equilibrium 2 – : : [Q] at equilibrium	x < 2 - x/	2			
	[r] <						
9.		A + B 💳	È C +	D			
	Initial At equili.	$\begin{array}{c} A + B \\ 1 \\ (1-x) \\ (1-x) \end{array}$	0 X	0 x			
		[C] [D]	X	x. x	0		
	÷	$K_{c} = \frac{[C] \ [D]}{[A] \ [B]} = 9$	÷	$(1-x)^2$	- = 9	or	$x^2 = 9 + 9x^2 - 18x$
	or	$8x^2 - 18x + 9 = 0$	<i>.</i>	$x = \frac{3}{2}$	or	$\frac{3}{4}$	
10.	Hence,	among the given option $N_2 + 3H_2 \rightleftharpoons 2$	-	otion (3)	i.e., 0.75	is corre	ect.
	t = 0	1 mole 2 mole	0				
	t = eq	1–x 2–3x	2x = 0.	8			
		x = 0.4 mole of N ₂ = 0.6	mole o	of $H_a = 0$.8		
		2		2			

Total mole of $PCl_3 = 0.7$

11.
$$K_{c} = \frac{\left(\frac{0.2}{2}\right)^{2} \times \left(\frac{0.8}{2}\right)}{\left(\frac{1}{2}\right)} = 0.04 \times 0.4 = 0.016$$

12.
$$PCI_5$$
 \implies PCI_3 + CI_2
1 0 0

Initial mole Conc. at equilibrium

Concentration = 0.14 $K_{c} = \frac{x^{2}}{(1-x)V} = \frac{0.7 \times 0.7}{0.3 \times 5} = \frac{49}{150}$ 19. $K_{p} = \frac{P'PCI_{3} \times P'CI_{2}}{P'PCI_{5}} = \frac{\frac{b}{(a+b+c)} \cdot P \times \frac{c}{(a+b+c)} \times P}{\frac{a}{(a+b+c)}P} \implies K_{p} = \frac{bc.P}{a \quad (a+b+c)}$

20.
$$P_{C_2} = 2.80 - (0.80 + 0.40) = 1.60$$
 atm,

$$k_{p} = \frac{P_{C_{2}}^{2}}{P_{A_{2}} \times P_{B_{2}}^{3}} = \frac{(1.60)^{2}}{0.80 \times (0.40)^{3}} = 50$$

21.
$$\frac{P_{SO_3}^2}{P_{SO_2}^2 \times P_{O_2}} = 4$$
, As $P_{SO_3} = P_{SO_2}$, $\frac{1}{P_{O_2}} = 4$ or $P_{O_2} = \frac{1}{4} = 0.25$ atm.

$$2NO_{2} \rightleftharpoons 2NO(g) + O_{2}(g)$$

$$K_{p} = \frac{(p_{NO})^{2} (p_{O_{2}})}{(p_{NO_{2}})^{2}}$$
given $P_{O2} = 0.25$; $P_{NO} = 0.5$
 $100 = \frac{(0.5)^{2} (0.25)}{(p_{NO_{2}})^{2}} \implies (P_{NO2})^{2} = \frac{(0.5)^{2} (0.25)}{100} \implies P_{NO2} = 0.025$

SECTION (C)

3.

22.

1.
$$Q_c = \frac{[C] [D]}{[A] [B]}, < K_c \quad \therefore Q_c$$
 with time

2. When $Q > K_c$, the reaction will proceed in backward direction to attain equilibrium.

$$N_2 + 3H_2 \implies 2NH_3, \quad K_P = 4.28 \times 10^{-5} \text{ atm}^{-2}$$

Reaction Quotient, $Q_P = \frac{P_{NH_3}^2}{P_{N_2}(PH_2)^3} = \frac{3^2}{1 \times (2)^3} = \frac{9}{8}$

 $Q_{P} > K_{P}$, \therefore Reaction will go Backward.

4.
$$Q = \frac{[C]^3}{[A]^2[B]} = \frac{(3/3)^3}{(2/3)^2(1/3)} = 6.75$$

 $Q < K_c$

The reaction will proceed in forward direction to attain equilibrium.

7.> $PCI_{5} \rightleftharpoons PCI_{3} + CI_{2}$ $\mathsf{K}_{\mathsf{P}} = \frac{\frac{(\alpha\mathsf{P})}{1+\alpha} \times \frac{(\alpha\mathsf{P})}{1+\alpha}}{\frac{1-\alpha}{1-\alpha} \times \mathsf{P}} = \frac{\alpha^2\mathsf{P}}{1-\alpha^2}$ $(\alpha < < 1)$ i.e. $\alpha \propto \frac{1}{\sqrt{P}}$ $x \propto \sqrt{V}$ or $x \propto \sqrt{16}$ Thus, 4 times 10. We know that d = $\frac{D}{1+(n-1)-\alpha}$ where n is number of mole of gases produced from one mole of a gas. 11. $\alpha = \frac{D-d}{(n-1)d} \implies n = \frac{1}{2}$ 12. $d_0 = \frac{D}{1 + (n - 1)\alpha} \Rightarrow \qquad n = 1 + \frac{1}{2} = 1.5 \qquad \Rightarrow \qquad 35 = \frac{40}{1 + 0.5\alpha} \Rightarrow \qquad 1 + 0.5\alpha = \frac{40}{35}$ 13. $0.5\alpha = 1.14 - 1$ $0.5\alpha = 0.14$ $\alpha = 0.28$ $\alpha = \frac{D-d}{(n-1)d} \implies \alpha = \frac{\frac{92}{2}-40}{(2-1)\cdot 40} = 0.15$ 14. SECTION (E) Homogenous reactions are those in which reactants and products are present in same phase. 1. $P_{NH_3} = P_{H_2S} = \frac{P}{2}$ Hence $K_p = P_{NH_3} \times P_{H_2S} = \frac{P}{2} \times \frac{P}{2} = \frac{P^2}{4}$ 2.> $NH_{a}HS(s) \Longrightarrow NH_{a}(g) + H_{a}S(g)$ 3. Р 2P = 1.2P = 0.6 $K_{p} = P^{2} = (0.6)^{2} = 0.36 \text{ atm}^{2}$ $\mathsf{K}_{\mathsf{P}} = \frac{[\mathsf{P}_{\mathsf{CO}}]^2}{\mathsf{P}_{\mathsf{CO}_2}}$ 4. $P_{CO} = P$ $P_{CO_2} + P_{CO} = 12$ P + 2P = 12P = 4 atm $P_{CO_2} = 4 \text{ atm}$ $K_{P} = \frac{8 \times 8}{4} = 16$ $K_c = [CO_2] = 0.05$ mole/litre 6. so moles of $CO_2 = 6.50 \times 0.05$ moles = 0.3250 moles $CaCO_3 \equiv CaO + CO_2$

1 mole of $CO_2 = 1$ mole of $CaCO_3$

0.3250 moles of $CO_2 = 0.3250$ moles of $CaCO_3 = 0.3250 \times 100$ gm of $CaCO_3 = 32.5$ gm of $CaCO_3$ SECTION (F)

- **1.** Gibbs equation $\Delta G = \Delta G^{\circ} RT \ln K$ at equilibrium $\Delta G = 0$ $-\Delta G^{\circ} = RT \ln K$
- **2.** At equilibrium $\Delta G = 0 \Rightarrow$ Given $\Delta G^0 = 0 \Rightarrow$ Gibbs equation $\Delta G = \Delta G^\circ RT \ln K$ $0 = 0 - RT \ln K \Rightarrow K = e^0 = 1$

3. So From equation it is given $T_2 > T_1 \therefore \left[\frac{1}{T_2} - \frac{1}{T_1}\right] = \frac{T_1 - T_2}{T_1 - T_2}$ = negative value

4. For endothermic reaction, ΔH^0 is positive so, if $T_2 > T_1$ then $K_2 > K_1$. For exothermic reaction, ΔH^0 is negative so, if $T_2 > T_1$ then $K_2 < K_1$.

5. \land T \uparrow K_c $\uparrow \Rightarrow$ Endothermic

SECTION (G)

- 1. On adding any reactant equilibrium shifts in forward direction, so amount of product increases.
- **2.** On adding inert gas at constant pressure effect on equilibrium will be similar to as if volume of container has been increased.
- **3.** For constant volume, reaction quotient (Q) will remain constant. For constant pressure, reaction quotient (Q) will remain constant when $\Delta n_a = 0$.
- 6. Since inert gas addition has no effect at const. volume.
- 7. For given reactions $\Delta ng = +ve$, $\Delta H = -ve$, high temperature & low pressure favours forward reaction which increases number of moles.

8. According to
$$K_{P} = \frac{P_{PCl_{3}}(g) \times P_{Cl_{2}}(g)}{P_{PCl_{5}}(g)} = \frac{(n_{PCl_{3}}(g))_{eq} \times (n_{Cl_{2}}(g))_{eq}}{V \times (n_{PCl_{5}}(g))_{eq}}$$

and on adding inert gas at constant pressure effect on equilibrium will be similar to as if volume of container has been increased.

- **11.** (1) Backward shifting will take place. (2) Forward shifting will take place.
 - (3) Backward shifting will take place. (4) Forward shifting will take place.
- **12.** Number of moles will remain unchanged but due to decreased volume pressure will get increased and also the concentrations.
- **13.** With change of pressure, x will change in such a way that K_p remains a constant.

14.

$\label{eq:N2O4} \begin{array}{c} \mathsf{N_2O_4} \mbox{ (g)} \mathchoice{\longleftarrow}{\longleftarrow}{\leftarrow} 2\mathsf{NO}_2. \end{array}$ moles t=0, 1 0 moles at eq. 1– α 2 α

$$K_{P} = \frac{\left(\frac{2\alpha}{(1+\alpha)} \times P\right)^{2}}{\frac{1-\alpha}{1+\alpha} \times P} = \frac{4\alpha^{2}}{1-\alpha^{2}} \times P.$$

Let total pressure at eq. = P. or $K_{P} = \frac{4\alpha^{2}}{1-\alpha^{2}} \times P.$

When volume is halved, P is double. $\therefore \alpha$ will change as K_P is independent of pressure change.

15. $H_2 \xrightarrow{Electricarc} 2H - 104.5$ kcal

atomic hydrogen

The reaction is endothermic. For endothermic reaction increase in temperature shift the equilibrium in forward direction. To proceed forward the pressure must be low because for the above reaction, increase of pressure will favoured backward reaction. So, for maximum yield the conditions are high temperature and low pressure.

SECTION (H)

- 1. A liquid and vapour is in equilibrium at its boiling point. The two phases have equal kinetic energy.
- 2. Since density of gold decreases after melting therefore it is favourable at low pressure and high temperature.
- **3.** Solublity of gas is favourable at high pressure and this process is exothermic hence solubility will be more at low temperature.
- 4. For any physical equilibrium on increasing pressure equilibrium shifts in the direction of higher density.

EXERCISE # 2

- **2.** At equilibrium, $r_f = r_b$ \therefore $K_f[A]_{en} = K_b[B]_{en}$ $[B]_{eq} = K_f K_b^{-1} [A]_{eq}$
- **3.** Equilibrium const. is temp. dependent only.

10. For pure solids & pure liquids, although they have their own active masses but they remain const, during a chemical change.

 $\rm K_{c}$ & $\rm K_{P}$ are equilibrium const. in terms of concentration & partical pressures. All options are correct.

12.
$$\log \left(\frac{K_p}{K_c} + \log RT = 0\right)$$

 $\log \left(\frac{K_p}{K_c} \cdot RT\right) = 0$
 $K_p = K_c (RT)^{-1} \quad \because K_p = K_c (RT)^{\lambda_0} \quad \Rightarrow \quad \Delta n = -1. \text{ This is possible for option (2)}$
13. $K_p = K_c (RT)^{-1} \quad \Delta n^2 4 - 3 = 1$
 $.052 K_c R \times 1000$
 $K_c = 5 \times 10^{-5} \times R^{-1}$
 $K_c = \frac{5 \times 10^{-5}}{R}$
14. $K_p = K_c (RT)^{-m} \quad \Delta n = -1$
 $\frac{K_p}{K_c} = \frac{1}{RT} = 0.0301.$
15. $\Delta K_c = \frac{|B|^2}{|A|} = \frac{(0.4)^2}{0.1} = 1.6$
16. $N_2 + O_2 \implies 2NO$
Initial 2 moles 4 moles
At Eq. $2 - \frac{1}{2}$ $4 - \frac{1}{2}$ $2 \times \frac{1}{2} = 1 \text{ mol}$
Molar concentration of NO at equilibrium $= \frac{1}{2.5} = 0.4$
17. $N_p + O_2 \implies 2NO$ $2x = 1.0 \text{ mole/litre}$
 $a = b = 0$ $x = 1.0/2 \text{ mole/litre} = 0.50 \text{ mole/litre}$
 $(a - x) (b - x) = 2x$
If $a - x = 0.25$, $b - x = 0.05$
 $[N_1] = a = a - x + x = 0.25 + 0.50 = 0.75 \text{ mole/litre}$
18. $PC_{I_q} \implies PC_{I_q} + C_{I_q}$
 $at t = 0 = a = 0 = 0$
 $t = t_{eq} = a - x \times x$
 $P_{PC_{I_q}} = PC_{I_q} + C_{I_q}$
20. $N_2O_5(g) \implies 2NO_2(g) + 1/2O_2(g)$
initial 600 0 0
 $eq. 600 (1 - \alpha) + 1200\alpha + 300\alpha = 980 \Rightarrow \alpha = 0.4$

21.	$A_2(g) + 2B_2(g) \implies 2C_2(g)$ $P_{A2} = 0.80 \text{ atm.}, \qquad P_{B2} = 0.4 \text{ atm.}$
	Total pressure of the system = 2.8 atm. $\therefore P_{C2} = 2.8 - 0.8 - 0.4 = 1.6$ $Kp = \frac{P_{C_2}^2}{P_{A_2} \times P_{B_2}^3} = \frac{(1.6)^2}{0.8 \times (0.4)^2} = 20$
22.	$N_2 + 3H_2 \implies 2NH_3, K_p = 4.28 \times 10^{-5} \text{ atm}^{-2}$
	Reaction Quotient, $Q_{P} = \frac{P_{NH_{3}}^{2}}{P_{N_{2}}(PH_{2})^{3}} = \frac{a}{1 \times (2)^{3}} = \frac{9}{8}$
	$Q_p > K_p$, \therefore Reaction will go Backward. $N_2 + 3H_2 \rightleftharpoons 2NH_3$, $K_p = 4.28 \times 10^{-5} \text{ atm}^{-2}$
23.	$Q_{c} = \frac{0.5 \times 0.1}{2^{2}} = \frac{.05}{.4} = 1.25 \times 10^{-2}$
	$K_c = 2 \times 10^{-2}$ $K_c > Q_c$ forward shiftment.
24.>	SO_2 + $\frac{1}{2}O_2$ \implies SO_3
	5 moles 5 moles 0
	$5-5 \times \frac{60}{100}$ $5-\frac{1}{2} \times 5 \times \frac{60}{100}$ $5 \times \frac{60}{100} = 2 + 3.5 + 3 = 8.5$ moles
25.>	$PCl_5 \Longrightarrow PCl_3 + Cl_2$
	α = .2, initially, $K_p = \frac{\alpha^2}{1 - \alpha^2} P = \frac{(0.2)^2}{1 - (.2)^2} \times 1 = \frac{.04}{.96} = .042$
	if $\alpha = .5$, thus, $\frac{(.5)^2}{1-(.5)^2} \times P = .042$, $P = .126$
26.>	$N_2O_4(g) \Longrightarrow 2NO_2(g)$
	initially, $t = 0$ a 0 a - a- α 2a α
	$a - a - \alpha$ $2a\alpha$ $K_p = \frac{4\alpha^2}{1 - \alpha^2}$ $P = 380 \text{ torr} = \frac{380}{760} = .5 \text{ atm}$
	$\frac{\alpha^2}{1-\alpha^2} = .335, \alpha^2 = .25, \alpha = .5$
27.	$N_2O_4(g) \implies 2NO_2(g)$
	$922 = (1 + \alpha) \times 61.33$
	$1 + \alpha = \frac{92}{61.33}$
	$\alpha = 0.5$
28.≿	$VD_{Minorobs} = \frac{D}{1 \times (n-1)d}$
	$VD_{obs} = 62, VD_{TH^2} = 104.16, n = 2$
	$\alpha = 68\%$
00	

29. (VD)_{mix} = $\frac{M_{mix}}{2} = \frac{M}{2(1+\alpha)}$

So, as α increases (VD)_{mix} decreases.

30. $PCl_{5}(g) \rightleftharpoons PCl_{3}(g) + Cl_{2}(g)$ 1 0 0 1-0.5 0.5 0.5 At equilibrium total mole = 1 - 0.5 + 0.5 + 0.5 = 1.5 $m_{mix} = m_{0} = \frac{M_{Initial}}{1 + (n - 1)\alpha}$ $m_{0} = \frac{208.5}{1 + (2 - 1) \times 0.5} = \frac{208.5}{1 + 0.5} = \frac{208.5}{1.5} = 139 \text{ g}$

 $\frac{1}{1+(2-1)\times 0.5} + \frac{1}{1+0.5} + \frac{1}{1.5}$ Density = $\frac{\text{Weight}}{\text{V}} = \frac{\text{Pm}_0}{\text{RT}} = \frac{2\times 139}{0.0821\times 800} = 4.232 \text{ g/L}$

31.
$$K_p = \frac{(p_{CO})^2}{p_{CO_2}} = \frac{(2)^2}{4} = 1.$$

$$C(s) + CO_2(g) \rightleftharpoons 2CO(g)$$

 $P-P/2 \qquad P = \frac{3P}{2} = 12$

So

$$K_{P} = \frac{P^{2}}{(P/2)} = 2P = 2 \times 8 = 16 \text{ atm.}$$

33. $K_p = 0.800$ atm = P_{CO_2} = maximum pressure of CO_2 in the container to calculate maximum volume of container the P_{CO_2} = 0.8 atm and none of CO_2 should get converted into $CaCO_3(s)$.

so V(0.800 atm) = (10 L) (0.2 atm) so V = 2.5 L

34.
$$K_p = P_{CO_2} = 8 \times 10^{-2}$$

$$k_{p} = \frac{(P_{CO})^{2}}{P_{CO_{2}}}$$
$$(P_{CO}) = \sqrt{K_{P} \times P_{CO_{2}}} = \sqrt{2 \times 8 \times 10^{-2}} = 4 \times 10^{-1}$$

- **35.** Slope = $\frac{-\Delta H^{\circ}}{2.3R}$ = $-\frac{230}{2.3 \times 2}$ = -50
- **38.** Addition of inert gas at constant volume has no effect on equilibrium concentrations.

39.
$$2A(s) + 3B(g) \rightleftharpoons 3C(g) + D(g) + O_2$$

If pressure on system is reduced to half its original value then equilibrium will shift in forward direction to increase no.of moles of gas to compensate reduction of pressure. \therefore Amounts of C & D will increase.

40. Upon addition of NH₃, 1st equilibrium will shift backward leading to decrease in amount of CO₂. As a result , 2nd equilibrium will shift forward compensating for the amount of decreased CO₂. So, n_{CaCO3} (s) will definitely decrease.

Now, $K_{P_1} = P^2_{NH_3} \times P_{CO_2} \& K_{P_2} = P_{CO_2}$

Since no change in temperature would have taken place, $K_{P_1} = K_{P_2}$ will have same values at both equilibrium states. So, amount of NH₃ & CO₂ at the two equilibrium states will remain the same.

41. A liquid and vapour is in equilibrium at its boiling point. The two phases have equal kinetic energy.

43. a T↓, then V↓, then P↑, equilibrium shift in such direction so as to decrease pressure, i.e., Backward direction.

EXERCISE # 3 PART - I

1. $BaO_2(s) BaO(s) + O_2(g)$; $\Delta H = + ve$ According to law mass action, the rate of forward reaction = r_1 $r_1 \propto [BaO_2]$ or $r_1 \propto k_1 [BaO_2]$

> But concentration of solid = 1 then, $r_1 = k_1$ similarly the rate of backward reaction = r_2

$$r_2 \propto [BaO] [O_2]$$
 or $r_2 \propto k_2 [BaO] [O_2]$

∴ conc. of [BaO] = 1

or $r_2 = k_2 [O_2]$

At equilibrium

$$r_1 = r_2$$

 $k_1 = k_2 [O_2]$ or $k_1 = k_2 \cdot p_{CO_2}$

where, p_{CO_2} = partial pressure of CO₂

or $\frac{k_1}{k_2} = p_{CO_2}$ (equilibrium constant) $\therefore \quad \frac{k_1}{k_2} = k$ or $k = p_{CO_2}$.

So, from the above it is clear that pressure of O_2 does not depend upon the concentration of reactants. The given equation is an endothermic reaction. If the temperature of such reaction is increased, then dissociation of BaO₂ would increase; and more O_2 is produced.

2.
$$k_{eq} = \frac{r_{f}}{r_{b}}$$
$$100 = \frac{10^{5}}{r_{b}}$$
$$r_{b} = 10^{3}$$

3. For reaction,
$$N_2(g) + 3H_2 \rightleftharpoons 2NH_3(g)$$

 $Q (Quotient) = \frac{[NH_3]^2}{[N_2][H_2]^3}$, $\Delta N = 2 - 4 = -2$

At equilibrium Q is equal to K_c but for the progress of reaction towards right side Q > K_c .

4.

5.

$$2NH_3 + \frac{5}{2}O_2 2NO + 3H_2O$$

$$2NH_{3} \rightleftharpoons 3H_{2} + N_{2} ; \qquad \frac{1}{K_{1}} \dots \dots \dots (1)$$

$$N_{2} + O_{2} \rightleftharpoons 2NO ; \qquad K_{2} \dots \dots \dots (2)$$

$$3H_{2} + \frac{3}{2} O_{2} \rightleftharpoons 3H_{2}O \qquad (K_{3})^{3} \dots \dots (3)$$
so on adding eq (1), (2) and (3)
we get $2NH_{3} + O_{2} \longrightarrow 2NO + 3H_{2}O$

$$3H_{2} + N_{2} \rightleftharpoons 2NH_{3}$$

At t=0	30	30	0
At t=t _{eq}	30–15	30–5	10

- **6.** Because K_{p} depends only on temperature. So, if then is constant, then K_{p} will also be constant.
- 7. Consider the eq. (i)

NO (g) +
$$\frac{1}{2}$$
 O₂ (g) \implies NO₂ (g)
 $K_1 = \frac{[N_2]^2 [O_2]}{[NO_2]^2}$
 $\frac{1}{K_1} = \frac{1}{\frac{[NO_2]}{[NO]} [O_2]^{1/2}} = \frac{[NO] [O_2]^{1/2}}{[NO_2]}$
 $\left(\frac{1}{K_1}\right)^2 = \left\{\frac{[NO] [O_2]^{1/2}}{[NO_2]}\right\}^2 = \frac{[NO]^2 [O_2]}{[NO_2]^2} = K_2$
 $\frac{1}{K_1^2} = K_2$

8. For the reaction, $CH_4 + 2O_2(g) \rightleftharpoons CO_2(g) + 2H_2O(\ell), \Delta_rH = -170.8 \text{ kJ mol}^{-1}$ This equilibrium is an example of heterogeneous chyemical equilibrium. Hence, for it

$$K_{c} = \frac{[CO_{2}]}{[CH_{4}] [O_{2}]}$$
(i)

(equilibrium constant on the basis of conc.)

and $K_p = \frac{p_{CO_2}}{p_{CH_4} \times p_{O_2^2}}$ (ii)

(equilibrium constant according to partial pressure)

Thus, in it concentration of CO_2 (g) and $H_2O(\ell)$ are not equal at equilibrium.

The equilibrium constant $(K_p) = \frac{[CO_2]}{[CH_4] [O_2]}$ is not correct expression.

1

On addition $CH_4 \iff (g)$ or $O_2(g)$ at equilibrium, K_c will be decreased according to expression (i) but K_c remains constant at constant temperature for a reaction, so for maintaining the constant value of K_c , the concentration of CO_2 will increased in same order. Hence, on addition of CH_4 or O_2 equilibrium will cause to the right.

This reaction is an example of exothermic reaction.

1

9.

$$HI (g) \iff \frac{1}{2} H_2(g) + \frac{1}{2} I_2(g)$$

$$K = \frac{[I_2]^{1/2} [H_2]^{1/2}}{[HI]} \qquad \dots \dots (i)$$

$$H_2(g) + I_2(g) \iff 2HI(g)$$

$$K' = \frac{[HI]^2}{[H_2] [I_2]} \qquad \dots \dots (ii)$$
From Eqs. (i) and (ii)

$$K \times \sqrt{K'} = 1$$

$$K' = \frac{1}{K^2} = \frac{1}{(8)^2} = \frac{1}{64}$$

10.	$Fe(OH)_{3}(s) \Longrightarrow Fe^{3+}(aq) + 3OH^{-}(aq) K = \frac{\left[Fe^{+3}\right] \left[OH^{-}\right]^{3}}{\left[Fe(OH)_{3}\right]} \qquad \qquad$
	To maintain equilibrium constant, let the concentration of Fe ³⁺ is increased x times, on decreasing the
	concentration of OH ⁻ by $\frac{1}{4}$ times K = $\frac{\left[xFe^{+3}\right]\left[\frac{1}{4}\times OH^{-}\right]^{3}}{\left[Fe(OH)_{3}\right]}$ (ii)
	From Eqs (i) and (ii) $\frac{1}{64} \times x = 1$
11.	$x = 64 \text{ times}$ $x \rightleftharpoons Y + Z$ $A \rightleftharpoons 2B$ $At t=0 1 0 0$ $At t=t_{eq} 1-\alpha \alpha \alpha$ $At t=t_{eq} 1-\alpha 2\alpha$
	$K_{P_1} = \frac{\frac{\alpha}{1+\alpha}P_1 \times \frac{\alpha}{1+\alpha}P_1}{\frac{1-\alpha}{1+\alpha}P_1} \dots \dots (i) \qquad \qquad K_{P_2} = \frac{\frac{4\alpha^2}{(1+\alpha)^2}P_2^2}{\frac{1-\alpha}{1+\alpha}P_2} \dots \dots (ii)$
	Divide equation (i) by (ii) we get :
	$\frac{K_{P_1}}{K_2} = \frac{1}{4} \frac{P_1}{P_2} \implies \frac{P_1}{P_2} = \frac{36}{1} \qquad \therefore \qquad P_1 : P_2 = 36 : 1$
12.	$2AB_2(g) \rightleftharpoons 2AB(g) + B_2(g)$
	$t = 0 \qquad 1 \qquad 0 \qquad 0$ $t = I_{eq} \qquad 1-x \qquad x \qquad \frac{x}{2}$
	-
	Total mole at eq = 1+ $\frac{x}{2}$
	$P_{AB_2} = \frac{1-x}{1+\frac{x}{2}} \times p \ , \ P_{AB} = \frac{1-x}{1+\frac{x}{2}} \times p \ , \ P_{B_2} = \frac{\frac{x}{2}}{1+\frac{x}{2}} \times p$
	Use $K_{p} = \frac{P_{B_{2}} \times (P_{AB})^{2}}{(P_{AB_{2}})^{2}}$ and neglect x as compare to 1, means 1-x 1
13.	Given, $CH_3COOH \Longrightarrow CH_3COO^- + H^+$; $K_a = 1.5 \times 10^{-5}$ (i)
	HCN \rightleftharpoons H ⁺ + CN ⁻ ; K _{a₁} = 4.5 × 10 ⁻¹⁰ (ii) CN ⁻ + CH ₂ COOH \rightleftharpoons HCN + CH ₂ COO ⁻ K = ?
	On subtracting Eq. (ii) from Eq. (i), we get $CH_3COOH + CN^- \Longrightarrow HCN + CH_3COO^-$
	$K = \frac{K_a}{K_{a_1}} = \frac{1.5 \times 10^{-5}}{4.5 \times 10^{-10}} = \frac{10^5}{3} = 3.33 \times 10^4$
14.	$2A_{(g)}$ + $B_{(g)}$ $3C_{(g)}$ + $D_{(g)}$
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	= 0.5 = 0.75 = 0.75 = 0.75 Equilibrium constant,
15.	$K = \implies K =$ When $K_p > Q$, rate of forward reaction > rate of backward reaction. \therefore Reaction is sontaneous.
	$p = \infty$, rate of forward reaction $r = rate of backward reaction. \dots Reaction is solitable us.$

When $\Delta G^{\circ} < RT$ In Q, ΔG° is positive, reverse reaction is feasible, thus reaction is non-spontaneous. When $K_p = Q$, rate of forward reaction = rate of backward reaction. \therefore Reaction is in equilibrium. When $T\Delta S > \Delta H$, ΔG will be negative only when $\Delta H = +$ ve.

16.
$$K_{p} = K_{c}(RT)^{\Delta n}$$

17. $N_2 + O_2 2NO$ K_1 (i) $2NO + O_2 2NO_2$ K_2 (ii) $NO_2 = \frac{1}{2}N_2 + O_2$ $K = \sqrt{\frac{1}{k_1 \cdot k_2}}$

18.
$$A_2 + B_2 \rightleftharpoons 2AB \qquad K_C$$

 $k_C = \frac{(2.8 \times 10^{-3})^2}{3 \times 10^{-3} \times 4.2 \times 10^{-3}} = \frac{(2.8)^2}{3 \times 4.2} = 0.62$

19. According to Le-Chatalier principle.

20.
$$\log \frac{K_2}{K_1} = \frac{\Delta H^0}{2.303 R} \left(\frac{1}{T_1} - \frac{1}{T_2} \right)$$

 $T_2 > T_1$ So $K_p < K_{P'}$ (exothermic reaction) (assuming $T_2 > T_1$, although it is not mentioned, which temprature is higher If $T_1 > T_2$ then $K_p > K_{P'}$ then answer should be (2).

21.
$$K = 1.6 \times 10^{12} = \left[\frac{\text{Product}}{\text{Reactant}}\right]$$

K have high value so products have very high conc than reactant.

22.
$$\Delta G^{\circ} = -2.303 \text{ RT} \log K$$

23. SrCO₃(s)
$$\rightleftharpoons$$
 SrO(s) + CO₂(g), Kp = 1.6 atm
Moles of CO₂ = $\frac{PV}{RT}$ = $\frac{0.4 \times 20}{RT}$ = $\frac{8}{RT}$
Kp = P_{CO2} = 1.6
P_{CO2} = $\frac{nRT}{V}$
1.6 = $\frac{\frac{8}{RT} \times RT}{V}$ \Rightarrow V = $\frac{8}{1.6}$ = 5L
24. 2NH₃ \rightleftharpoons N₂ + 3H₂ $\frac{1}{K_1^2}$
N₂ + O₂ \rightleftharpoons 2NO K₂
3H₂ + $\frac{3}{2}$ O₂ \rightleftharpoons 3H₂O
 $\frac{1}{2NH_3 + \frac{5}{2}}$ O₂ \xleftarrow{K} 2NO + 3H₂O

$$\mathsf{K} = \frac{\mathsf{K}_2 \mathsf{K}_3^3}{\mathsf{K}_1^2}$$

25. $A_2(g) + B_2(g) \Longrightarrow x_2(g)$ $\Delta H_r = -X kJ$

 $\underline{\Delta}n_g = -ve \& \underline{\Delta}H = -ve$ (exothermic reaction) so ideal condition for formation of product is High pressure & low temperature.

26. For the chemical reaction

Rate of reaction =
$$-\frac{d(N_2)}{dt} = -\frac{1}{3}\frac{d[H_2]}{dt} = \frac{1}{2}\frac{d(NH_3)}{dt}$$

PART - II

1. $I_2(g) \Longrightarrow 2I(g), \Delta H^{\circ}_{r}(298 \text{ K}) = +150 \text{ kJ}$

According to Le-Chatelier's principle the condition favouring formation of I are

- (i) High concentration of I_2
- (ii) High temperature (reaction is endothermic so, on increasing the temperature equilibrium will shift in the direction where heat is absorbed).
- (iii) Low pressure (moles of products are more than moles of reactant, so if pressure is increased equilibrium will shift in the direction where volume is less.)

D (g)

3. For a reaction,
$$K_c = \frac{[Pr oduct]}{[Reactant]}$$
. Hence, if

if $K_c > 1$, then [Product] > [Reactant].

equilibrium)

4.
$$K_c = \frac{[NH_3]^2}{[N_2] [H_2]^3}$$

$$K_{c} = \frac{\text{mol}^{2} \times L \times L^{3}}{L^{2} \times \text{mol} \times \text{mol}^{3}} = L^{2} \text{ mol}^{-2}$$

A (g) + B (g)

7.

$$\sum_{\substack{(2-3x) \\ = x \\ =$$

C (g)

6.
$$2NO + O_2 \rightleftharpoons 2NO_2$$

In this reaction,

Number of moles of gaseous reactants, $n_1 = 3$

Number of moles of gaseous products $n_p = 2$

Since, n_p is less than n_r , according to Le-Chatelier principle, increase in pressure shifts the equilibrium in forward direction, ie, more NO₂ is formed.

The reaction given above is exothermic.

From given equations

We have

$$K_1 = \frac{[NH_3]^2}{[N_2][H_2]^3} \implies K_2 = \frac{[NO]^2}{[N_2][O_2]} \implies K_3 = \frac{[H_2O]}{[H_2][O_2]^{1/2}}$$

For the given reaction

$$\mathsf{K} = \frac{[\mathsf{NO}]^2 \, [\mathsf{H}_2 \mathsf{O}]^3}{[\mathsf{NH}_3]^2 \, [\mathsf{O}_2]^{5/2}} \qquad \Rightarrow \qquad \frac{\mathsf{K}_2 \mathsf{K}_3^3}{\mathsf{K}_1} = \frac{[\mathsf{NO}]^2 \, [\mathsf{H}_2 \mathsf{O}]^3}{[\mathsf{NH}_3]^2 \, [\mathsf{O}_2]^{5/2}} \Rightarrow \qquad \mathsf{K} = \frac{\mathsf{K}_2 \mathsf{K}_3^3}{\mathsf{K}_1}$$

8. $3Fe(s) + 4H_2O(stream) = Fe_3O_4(s) + 4H_2(g)$

$$K_{p}=\frac{\left(p_{H_{2}}\right)^{4}}{\left(p_{H_{2}O}\right)^{4}}$$
 only gaseous products and reactants.

17. 2ICI = l₂ + Cl_2

0.6

$$0.6 - 2x \qquad x \qquad x \qquad x \qquad x \qquad K_{C} = 0.14 = \frac{x^{2}}{(0.6 - 2x)^{2}}$$
$$0.37 = \frac{x}{0.6 - 2x} \qquad 0.224 - 0.748 \ x = x \qquad 1.748x = 0.224 \qquad x = 0.128$$

18.

	A +	2B ₹	≥ 2C
initial mole	2	2	0
at equilibrium mole	2 – x	2–2x	2x
	1.5	1	1
	15	1	1

10

10

equilibrium conc.

$$K_{C} = \frac{\left[C\right]^{2}}{\left[A\right] \left[B\right]^{2}}$$
$$= \frac{\left[\frac{1}{10}\right]^{2}}{\left[\frac{15}{10}\right] \left[\frac{1}{10}\right]^{2}} = 6.67$$

C form 1 mole at equilibrium 2x = 1 $x = \frac{1}{2} = 0.5$

 $\mathsf{K}_{\mathsf{P}} = \mathsf{P}_{\mathsf{CO}_2} \, .$ 19.

Pressure will increase only by increasing temperature as it will change K_P value.

1

10

PART - III

- 1. In this reaction the ratio of number of moles of reactants to products in same i.e., 2:2, hence change in volume will not alter the number of moles .
- 2. If in the reaction the ratio of number of moles of reactants to products in same i.e., 1:1, then change in volume will not alter the number of moles .
- The conversion of SO₂ to SO₃ is an exothermic reaction, hence there is no need to increase the 3. temperature. There is also a decrease in volume or moles in product side. Thus the reaction is favoured by low temperature and high pressure. (Le-Chatelier's principle).

4.
$$C_{[N_2O_4]} = 4.8 \times 10^{-2} \text{ mol } L^{-1}, \ C_{[NO_2]} = 1.2 \times 10^{-2} \text{ mol } L^{-1}$$

 $K_c = \frac{[NO_2]^2}{[N_2O_4]} = \frac{1.2 \times 10^{-2} \times 1.2 \times 10^{-3}}{4.8 \times 10^{-2}} = 0.3 \times 10^{-2} = 3 \times 10^{-3} \text{ mol } L^{-1}$
5. $P_4(g) + 5O_2(g) \Longrightarrow P_4O_{10}(g) \qquad K_c = \frac{[P_4O_{10}(s)]}{[P_4(s)][O_2(g)]^5}$

6.	$CO(g) + Cl_2(g) \implies COCl_2(g)$	
	$\Delta n = 1 - 2 = -1; \ K_p = K_c(RT)^{\Delta n} \ :.$	$\frac{K_{p}}{K_{c}} = (RT)^{-1} = \frac{1}{RT}$
7.	$N_2(g) + O_2(g) \implies 2NO(g)$;	$K_c = \frac{[NO]^2}{[N_2][O_2]} = 4 \times 10^{-4}$
	$NO(g) \rightleftharpoons \frac{1}{2} N_2(g) + \frac{1}{2} O_2(g);$	$K_{c} = \frac{[N_{2}]^{1/2}[O_{2}]^{1/2}}{[NO]} = \frac{1}{\sqrt{K_{c}}} = \frac{1}{\sqrt{4 \times 10^{-4}}} = \frac{1}{2 \times 10^{-2}} = \frac{100}{2} = 50$
8.	$\begin{split} & K_{p} = K_{c} \; (RT)^{\Delta n} & \Delta n = 3 - 2 = 1. \\ & K_{p} = K_{c} \; (0.0821 \times 457)^{1} \; . \; K_{p} > K_{c}. \end{split}$	
9.	$CI_2(g) + 3F_2(g) \implies 2CIF_3(g); \Delta H = -$ (i) Decrease in temperature, (ii) Addition	329 kJ. Favourable conditions: n of reactants, (iii) Increase in pressure i.e., decrease in volume.
10.	$\begin{split} & NH_4HS(s) \mathchoice{\longrightarrow}{\leftarrow}{\leftarrow}{\leftarrow} NH_3(g) \\ & Initial presens 0 \qquad 0.5 \\ & At equi. \qquad 0 \qquad 0.5 + x \\ & Total pressure = 0.5 + 2x = 0.84 \\ & K_{p} = P_{NH_3} \times P_{H_2S} = 0.11 \ \mathrm{atm}^2. \end{split}$	0
11.	Given : $PCI_{5}(g) \rightleftharpoons PCI_{3}(g)$ t = 0 1 0 t_{eq} 1-x x Total number of moles = 1 - x + x + x = Thus partial pressure of $PCI_{3}\left(\frac{x}{1+x}\right) = 1$	0 x 1 + x
12.	$SO_3(g) \iff SO_2(g) + \frac{1}{2} O_2(g)$	
	$\frac{[SO_2][O_2]^{1/2}}{[SO_3]} = K_c = 4.9 \times 10^{-2}$	(i)
	$SO_3(g) + 1/25 O_2(g) \Longrightarrow SO_3(g)$	(ii)
	$\frac{[SO_3]}{[SO_2][O_2]^{1/2}} = K'_c = \frac{1}{4.9 \times 10^{-2}} \text{ For } 2S$	$O_2(g) + O_2(g) \rightleftharpoons 2SO_3(g)$
	$\frac{[SO_3]^2}{[SO_2]^2[O_2]} = K_c^2 = \frac{1}{4.9 \times 4.9 \times 10^{-4}} = \frac{1}{4.9 \times 4.9 \times 10^{-4}}$	$\frac{10000}{24.01} = 416.49$
13.	c = a + b	

14. $X \implies 2Y$ $Z \implies P + Q$ $1-\alpha$ 2α $1-\alpha \qquad \alpha$ $K_{p_{1}} = \frac{\left(\frac{2\alpha}{1+\alpha}P_{T_{1}}\right)^{2}}{\left(\frac{1-\alpha}{1+\alpha}P_{T_{1}}\right)} \qquad \qquad K_{p_{2}} = \frac{\left(\frac{\alpha}{1+\alpha}P_{T_{2}}\right) \cdot \left(\frac{\alpha}{1+\alpha}P_{T_{2}}\right)}{\left(\frac{1-\alpha}{1+\alpha}P_{T_{2}}\right)}$ $\frac{\mathsf{K}_{\mathsf{P}_{1}}}{\mathsf{K}_{\mathsf{P}_{2}}} = \frac{\left(\frac{2\alpha}{1+\alpha}\mathsf{P}_{\mathsf{T}_{1}}\right)^{2}}{\left(\frac{1-\alpha}{1+\alpha}\mathsf{P}_{\mathsf{T}_{2}}\right)} \times \frac{\left(\frac{1-\alpha}{1+\alpha}\mathsf{P}_{\mathsf{T}_{2}}\right)}{\left(\frac{\alpha}{1+\alpha}\mathsf{P}_{\mathsf{T}_{2}}\right) \left(\frac{\alpha}{1+\alpha}\mathsf{P}_{\mathsf{T}_{2}}\right)}$ $\frac{1}{9} = \frac{4P_{T_1}}{P_{T_2}} ; \qquad \qquad \frac{P_{T_1}}{P_{T_2}} = \frac{1}{36}$ 15. PV = nRT $V = 1 \text{ dm}^3 = 10^{-3} \text{ m}^3$

P = 3170 Pa R = 8.314 J K⁻¹ mol⁻¹ T = 300 K $3170 \times 10^{-3} = n \times 8.314 \times 300$ $n = \frac{3170 \times 10^{-3}}{8.314 \times 300} = 1.27 \times 10^{-3} \text{ mol.}$

16.
$$CO_2(g) + C(s) = 2CO(g)$$

0.5 atm
0.5-p 2p
Total pressure = $0.5 - P + 2P = 0.8$
 $P = 0.3$
 $K_p = \frac{P_{CO}^2}{P_{CO_2}} = \frac{(2P)^2}{(0.5 - P)} = \frac{(0.6)^2}{(0.5 - 0.3)}$
 $K_p = 1.8$

 $\mathbf{K}_{p} = \mathbf{K}_{c} \ \left(\mathbf{RT} \right)^{\Delta n_{g}}$ 17. $\Delta n_g = -\frac{1}{2}$

 $\Delta G = \Delta G^{\circ} + RT \ln Q = 2494.2 + 8.314 \times 300 \ln 4 = positive$ 18. $\Delta G = RT \ell n \ \frac{Q}{\kappa}$

Since, ΔG is positive so, Q > K, so reaction shifts in reverse direction.

19.

•	t = 0 t _{eq}	A 1 1–x	+ B 1 1–x	~	C 1 1 + x	+ 1	D 1 1 + x	
		\Rightarrow	$\frac{(1+x)^2}{(1-x)^2}$	= 100		\Rightarrow	$\frac{1+x}{1-x} = 10$	
		\Rightarrow	1 + x = 1	0 – 10x		\Rightarrow	11x = 9	
		\Rightarrow	$x = \frac{9}{11}$			\Rightarrow	$[D] = 1 + \frac{9}{11}$	
		\Rightarrow	[D] = 1.8	18				

20.	(A & B)
	$\ell n K = \ell n A - \frac{\Delta H}{R} \times \frac{1}{T} \implies Slope = -\frac{\Delta H}{R}; \Delta H = -ve$
21.	$(2) = 3 \times (-(1)) \therefore \mathbf{K}_2 = \left(\frac{1}{\mathbf{K}_1}\right)^3 \implies \mathbf{K}_2 = \mathbf{K}_1^{-3}$
22.	$k_{P}/k_{c} = (RT)^{\Delta n_{g}}$
	(1) $\Delta n_g = 0 \qquad \Rightarrow \qquad \frac{k_p}{k_c} = 1$
	(2) $\Delta n_g = 2 - 1 = 1 \qquad \Rightarrow \qquad \frac{k_p}{k_c} = (RT)^1 = (24.62)^1$
	(3) $\Delta n_g = 2 - 4 = -2 \qquad \Rightarrow \qquad \frac{k_p}{k_c} = (RT)^{-2} = (24.62)^{-2} = 1.65 \times 10^{-3}$
23.	$\begin{array}{rcl} NH_4HS & \longrightarrow & H_2S & + & NH_3\\ 0.1(1-0.3) & & 0.03 & & 0.03 \end{array}$
	$K_{\rm C} = \frac{0.03}{3} \times \frac{0.03}{3} = 10^{-4} \implies \qquad K_{\rm P} = K_{\rm C} \ ({\rm RT})^{\Delta n} = 10^{-4} \times (0.0821 \times 600)^2 = 0.242$
24	$2NH_3 \longrightarrow N_2 + 3H_2 K'_P = \frac{1}{k_p}$
	$P_{\text{Total}} = P = P_{N_2} + P_{H_2} + P_{NH_3} \simeq P_{N_2} + P_{H_2}$
	$P_{N_2} = \frac{P}{4} \qquad \Rightarrow \qquad P_{H_2} = \frac{3P}{4} \qquad \Rightarrow \qquad \frac{1}{k_P} = \frac{\left(\frac{P}{4}\right)\left(\frac{3P}{4}\right)^3}{\left(P_{NH_2}\right)^2} \Rightarrow \qquad P_{NH_3} = \frac{3^{\frac{3}{2}}P^2}{16} (k_P)^{1/2}$
25.	$A + 2B \implies 2C + D$
	initially conc. a 1.5a at eq. a-x 1.5 a–2x 2x x
	at equilibrium $a-x = 1.5a - 2x$ 0.5 $a = x$
	a = 2x
	$k_{\rm C} = \frac{(2x)^2(x)}{(a-x)(1.5a-2x)^2} = \frac{4x^2 \cdot x}{(x)(x)^2} = 4$
26.	$A(s) \Longrightarrow B(g) + C(g)$ $k_{P_1} = x \text{ atm}^2$
	$P_1 \qquad P_1 + P_2$ $D(s) \longleftrightarrow C(g) \qquad + E(g) \qquad k_{P_2} = y \text{ atm}^2$
	$P_1 + P_2 = P_2$
	$k_{P_1} = P_1(P_1 + P_2)$
	$k_{P_2} = P_2(P_1 + P_2)$
	$k_{P_1} + k_{P_2} = (P_1 + P_2)^2$
	$x + y = (P_1 + P_2)^2 \implies P_1 + P_2 = \sqrt{x + y}$
	$2(P_1 + P_2) = 2\sqrt{x + y}$
	$P_{Total} = P_B + P_C + P_E = 2(P_1 + P_2) = 2\sqrt{x + y}$